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# Fuji IGBT Module V Series 1200V Family

## Technical Notes

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# - Fuji IGBT Module V Series 1200V Family-

## RBSOA and SCSOA

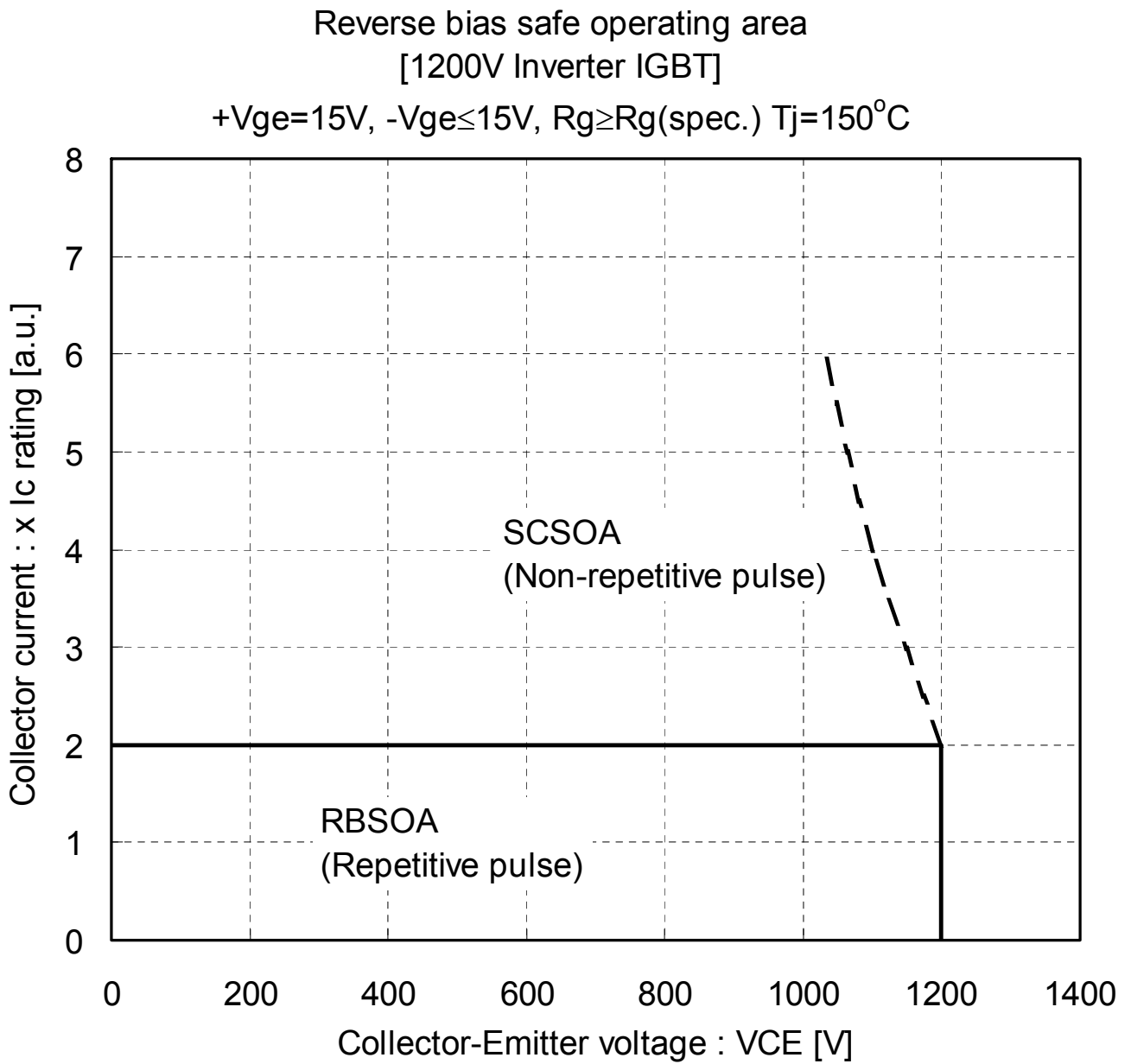


Fig. RBSOA and SCSOA

Technical data: MT5F24325

# - Fuji IGBT Module V Series 1200V Family -

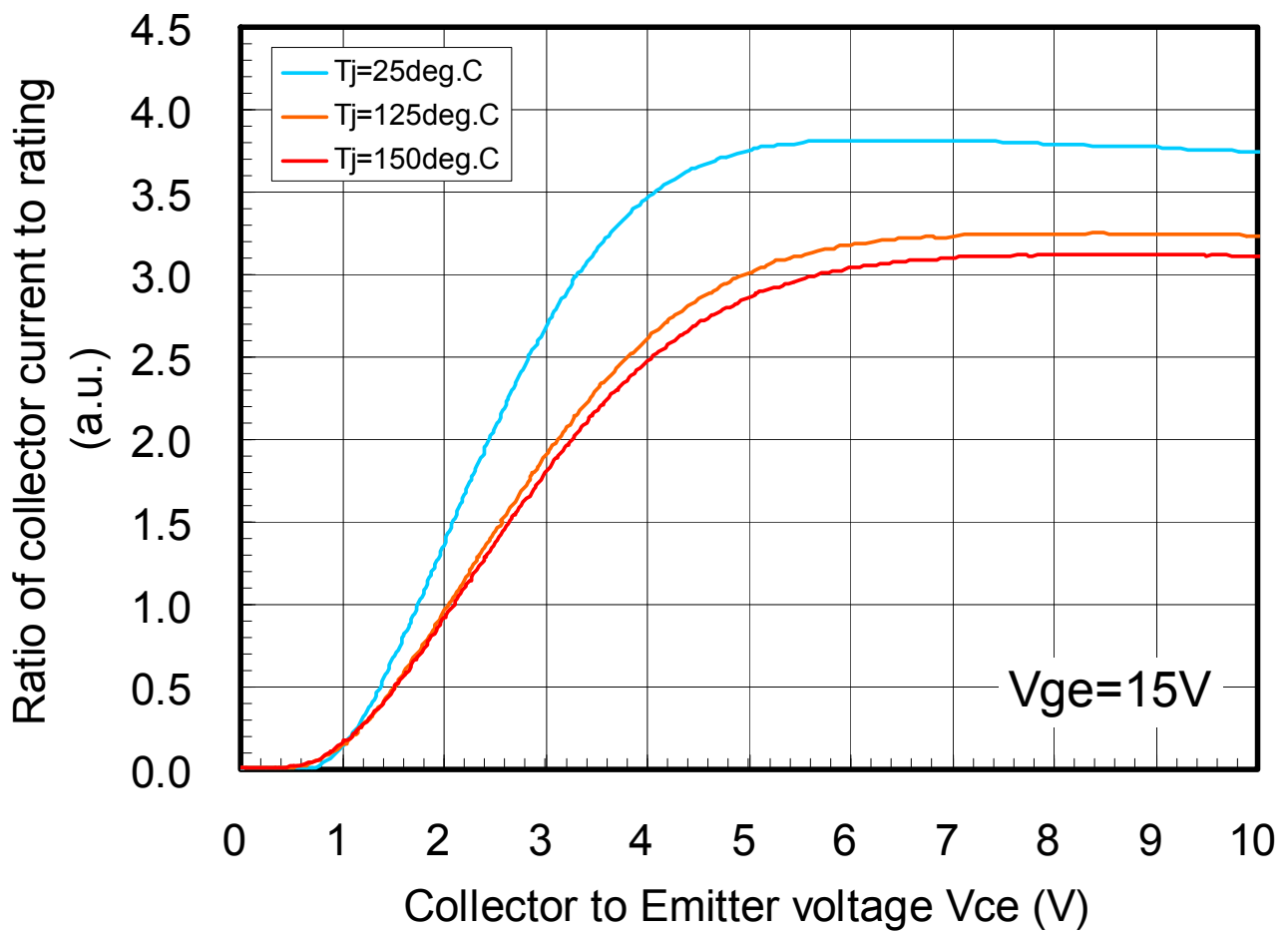
## High current output characteristics

V series 1200V product family

Conditions:  $T_j = 25^\circ\text{C}$ ,  $125^\circ\text{C}$  and  $150^\circ\text{C}$

$V_{ge} = 15\text{ V}$

Note: This data shows the typical waveforms of chip characteristics. The effect of the internal resistance of the module is not included



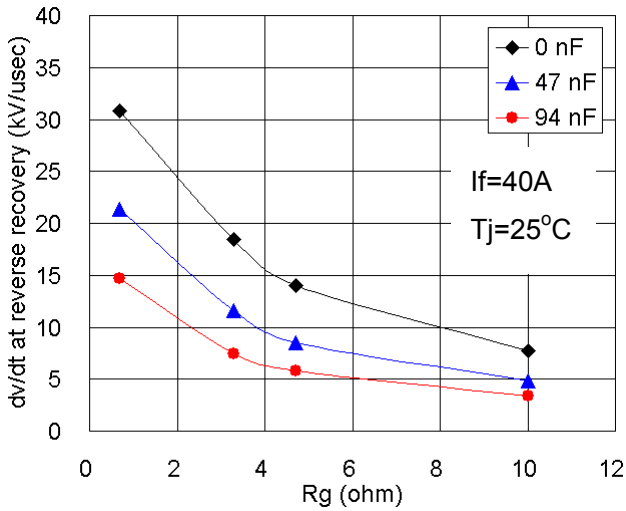
Technical data: MT5F24326

# – Fuji IGBT Module V Series 1200V Family –

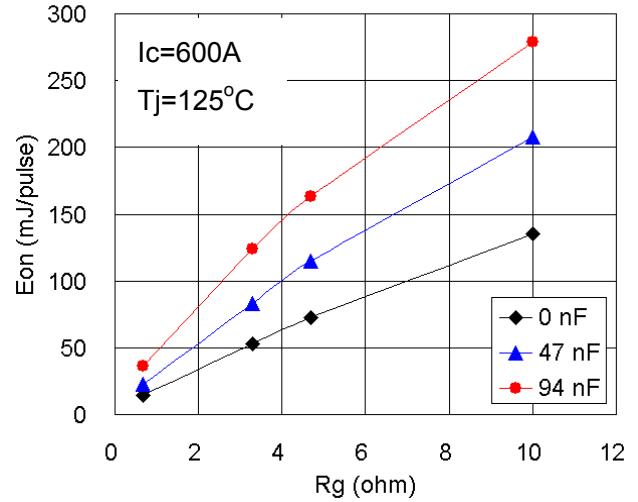
## Switching energy and Reverse recovery $dv/dt$ with combination of $R_g$ and $C_{ge}$

Type name: 2MBI600VN-120-50

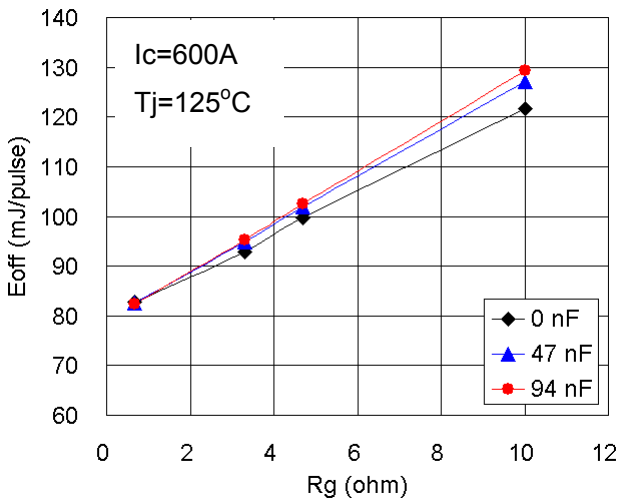
Conditions:  $V_{dc}=600V$ ,  $I_c$ ,  $I_f=40A$  and/or  $600A$ ,  $V_{ge}=+/-15V$ ,  $C_{ge}=0, 47, 94nF$ ,  
 $T_j=25^\circ C$  or  $125^\circ C$



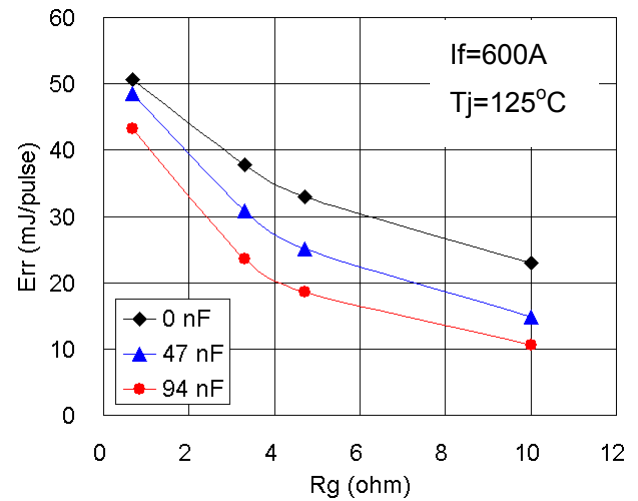
(a)  $R_g$  dependence of reverse recovery  $dv/dt$



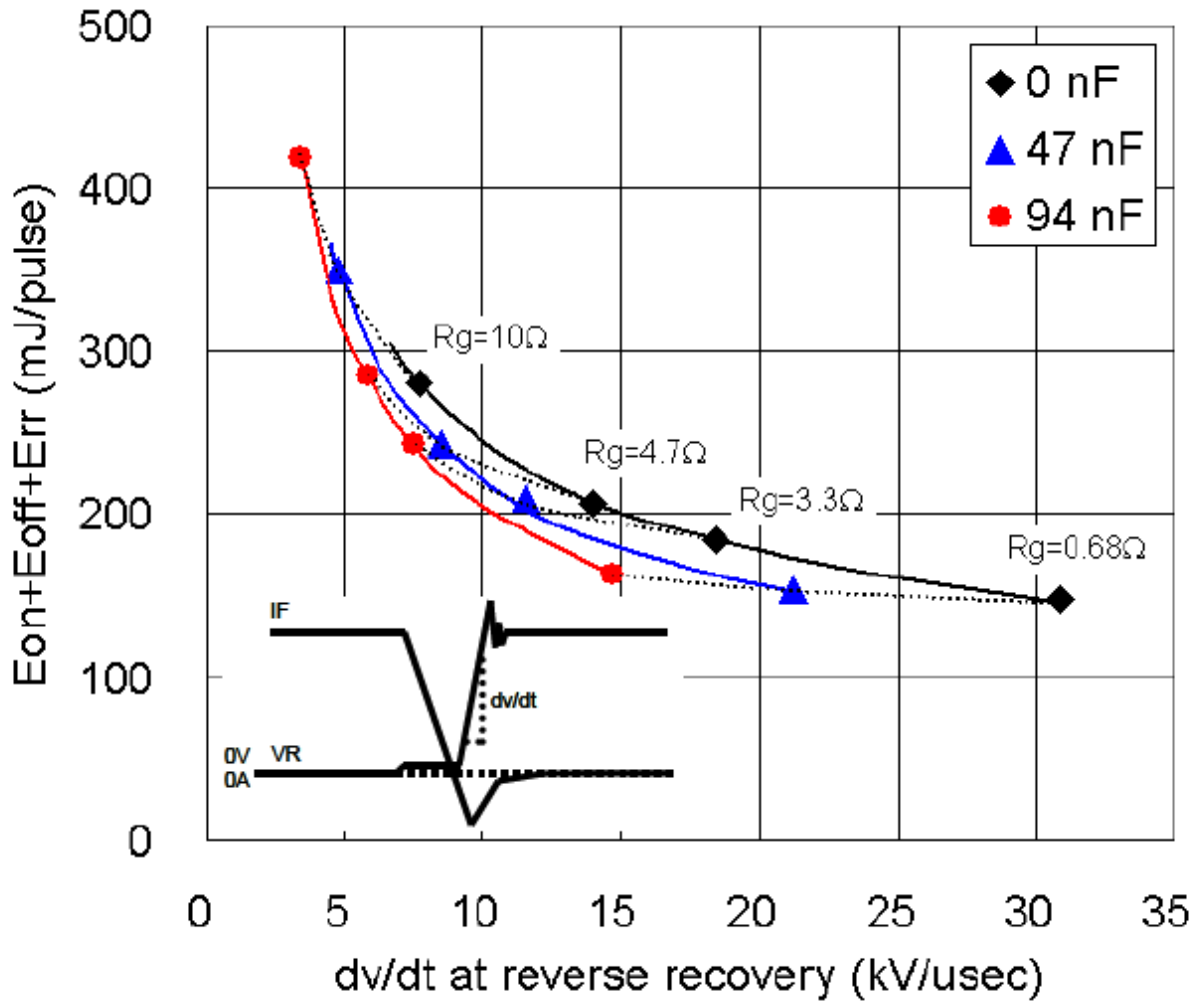
(b)  $R_g$  dependence of turn-on loss



(c)  $R_g$  dependence of turn-off loss



(d)  $R_g$  dependence of reverse recovery loss



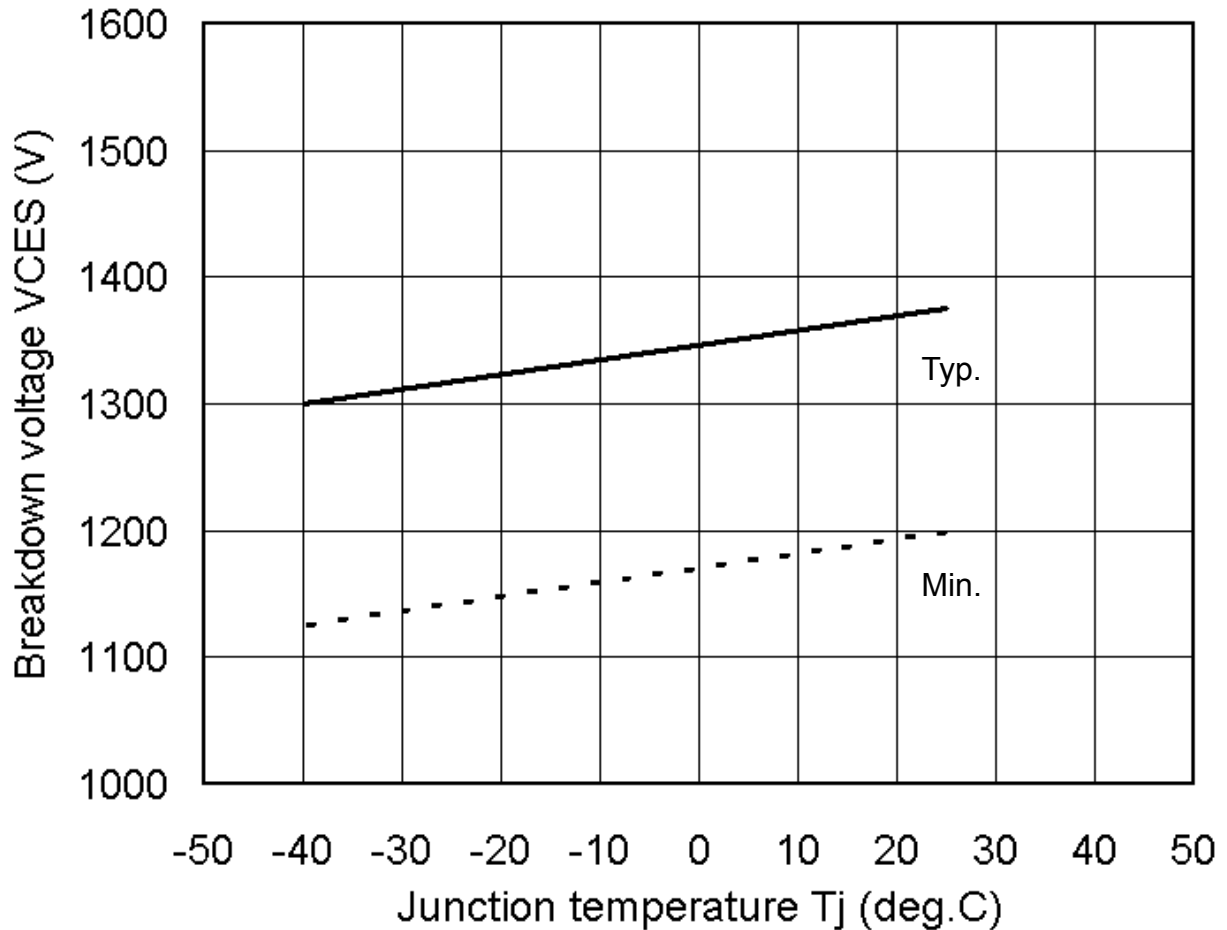
Cge and Rg Dependence for Sum of Switching Loss and Reverse Recovery dv/dt

Additional external capacitance between IGBT gate and emitter terminals has an effect of improving the trade off between reverse recovery  $dv/dt$  and total switching energy as shown in above chart. However, simply add  $C_{ge}$  slows down the IGBT significantly and it results penalty of increasing the switching loss. Therefore, the combination of extra- $C_{ge}$  and reduction of the gate resistance ( $R_g$ ) is recommended to achieve the highest performance of lower  $dv/dt$  as well as keep switching energy low. Typical  $C_{ge}$  and  $R_g$  values for initial guess are : 2x of  $C_{ies}$  in our datasheet and 1/2  $R_g$  of your original design, however, experimental confirmation in practical application is recommended,

Technical data: MT5F21212

# – Fuji IGBT Module V Series 1200V Family –

## Junction breakdown voltage $V_{CES}$ and junction temperature $T_j$



Junction Temperature Dependence of Junction Breakdown Voltage

In General, the breakdown voltage of power semiconductor devices have liner function to the junction temperature if "impact ionization" and "Avalanche multiplication" are dominant physics of junction breakdown. At low temperature, the carriers in drift region are relatively easier to have high velocity because of less scattering due to lattice vibration so that the impact ionization ratio increases. Therefore, the breakdown voltage of the power semiconductor device becomes lower at low temperature. The temperature effect shown in the above figure should be taken into account into practical design not to exceed breakdown voltage if the target application have chances of low temperature operation and/or start-up.

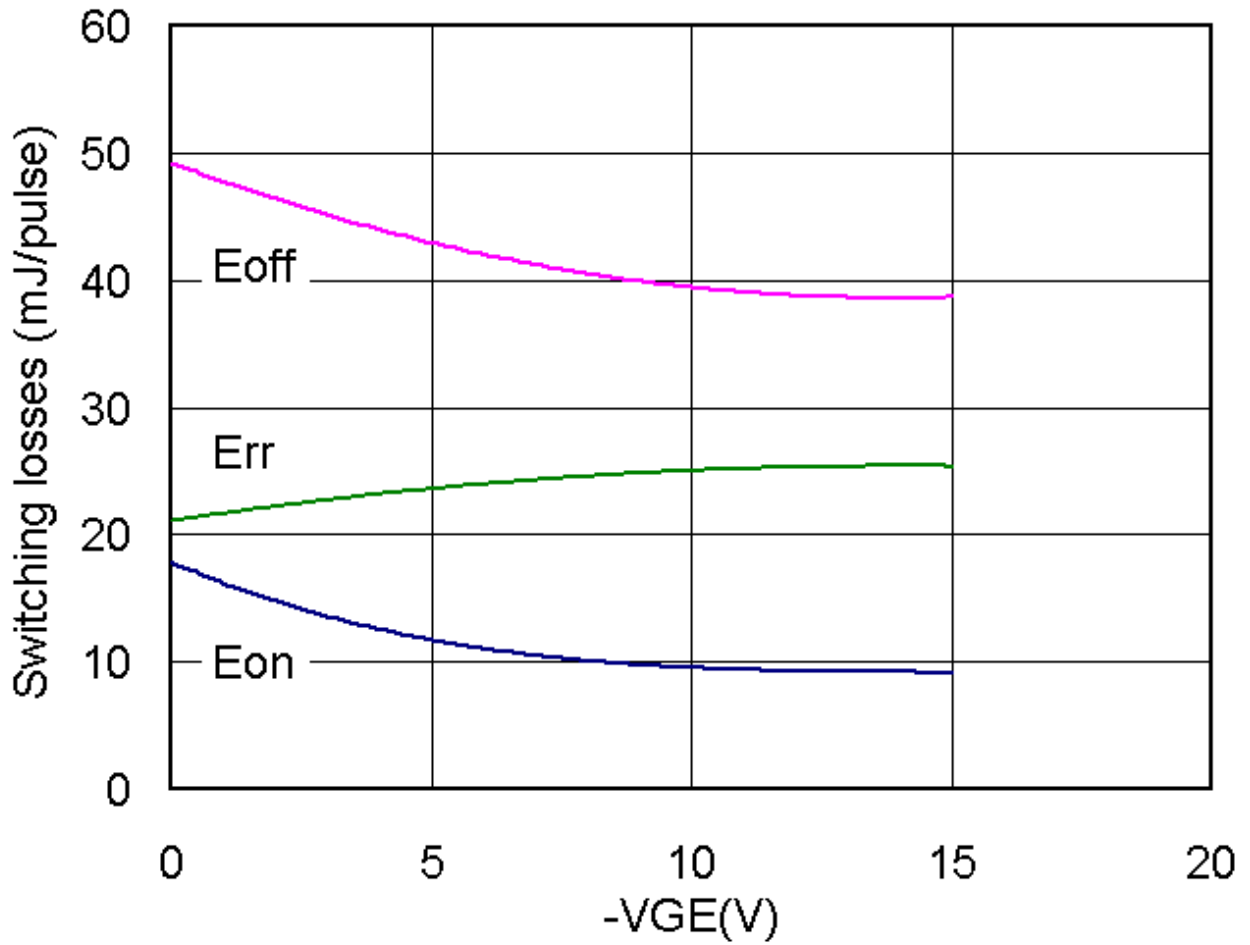
Technical data: MT5F24327

# - Fuji IGBT Module V Series 1200V Family -

## -Vge and switching loss characteristics

Type name: 2MBI300VN-120-50

Conditions: Vdc=600V, Ic=300A, Vge=+15V, Rg=0.92Ω



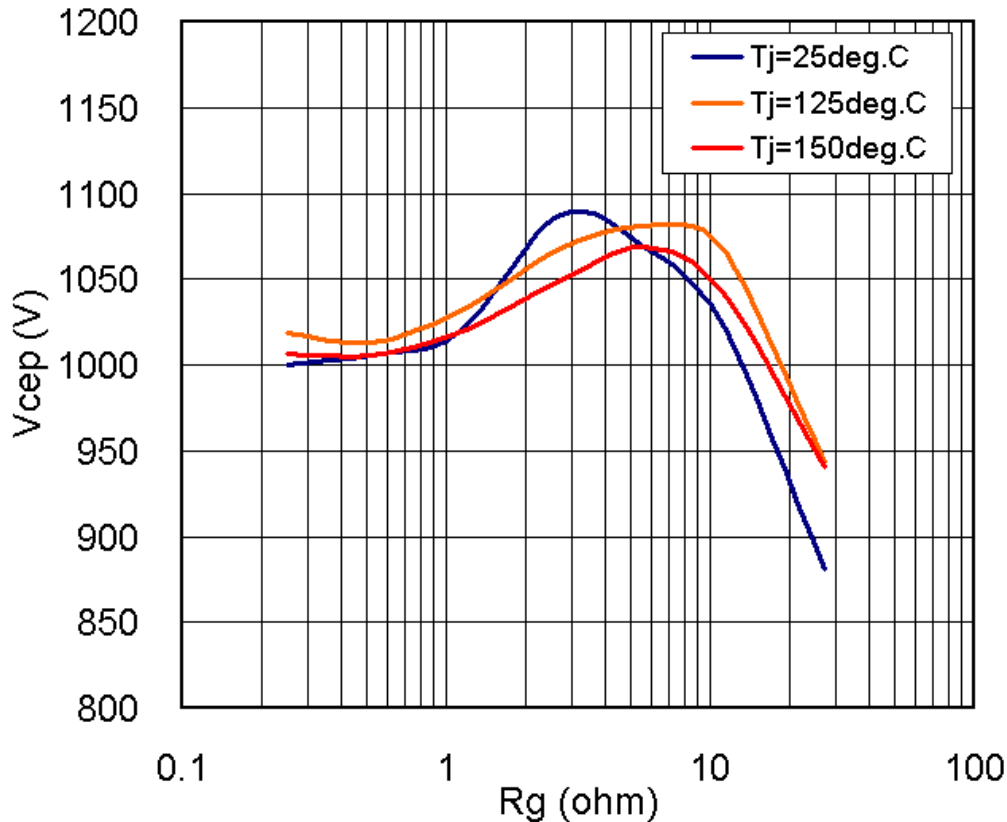
Technical data: MT5F21212

# – Fuji IGBT Module V Series 1200V Family –

## Gate resistance dependence of surge voltage

Type name: 2MBI450VN-120-50

Conditions:  $V_{dc}=600V$ ,  $I_c=450A$ ,  $V_{ge}=\pm 15V$ ,  $L_s=70nH$ ,



Gate Resistance Dependence of Turn-off Surge Voltage

The surge voltage, especially at IGBT turn off, depends on the gate resistance. As shown in the figure above, the surge voltage can be controlled with the gate resistance, but the curves have peaks depending on the junction temperature. Although detailed reasons for this relation are not described here, the background of such behaviors has already been analyzed and published. The primary reason for such behavior is the interaction of two silicon physics in IGBT chip; 1) the carriers stored in the drift region and 2) Current through MOS channel<sup>1)</sup>.

This chart also indicates that increasing the gate resistance is not only the method to solve the turn-off spike voltage issue. The decrease of the gate resistance may also have an effect.

Reference :

- 1) Y. Onozawa et al., "Investigation of carrier streaming effect for the low spike fast IGBT turn-off", Proc. ISPSD, pp173-176, 2006.

Technical data: MT5F24328



# - Fuji IGBT Module V Series 1200V Family -

## - $-di_c/dt$ at turn-off and $T_j$ characteristics

- 2MBI600VN-120-50

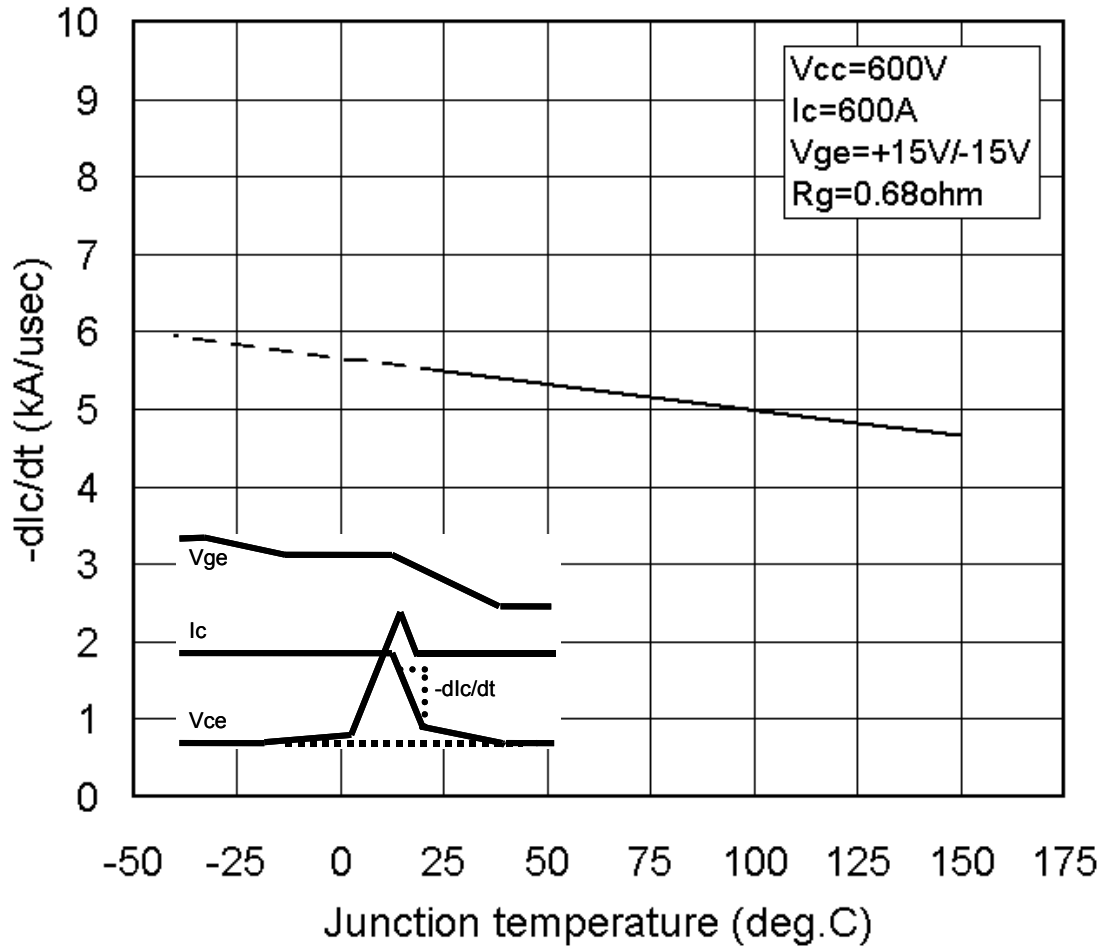


Fig.  $-di_c/dt$  at Turn-Off and  $T_j$  Characteristics

Technical data: MT5F24329

# - Fuji IGBT Module V Series 1200V Family -

## Dynamic avalanche voltage $V_{av}$ and $T_j$ characteristics

Type name: 2MBI600VN-120-50

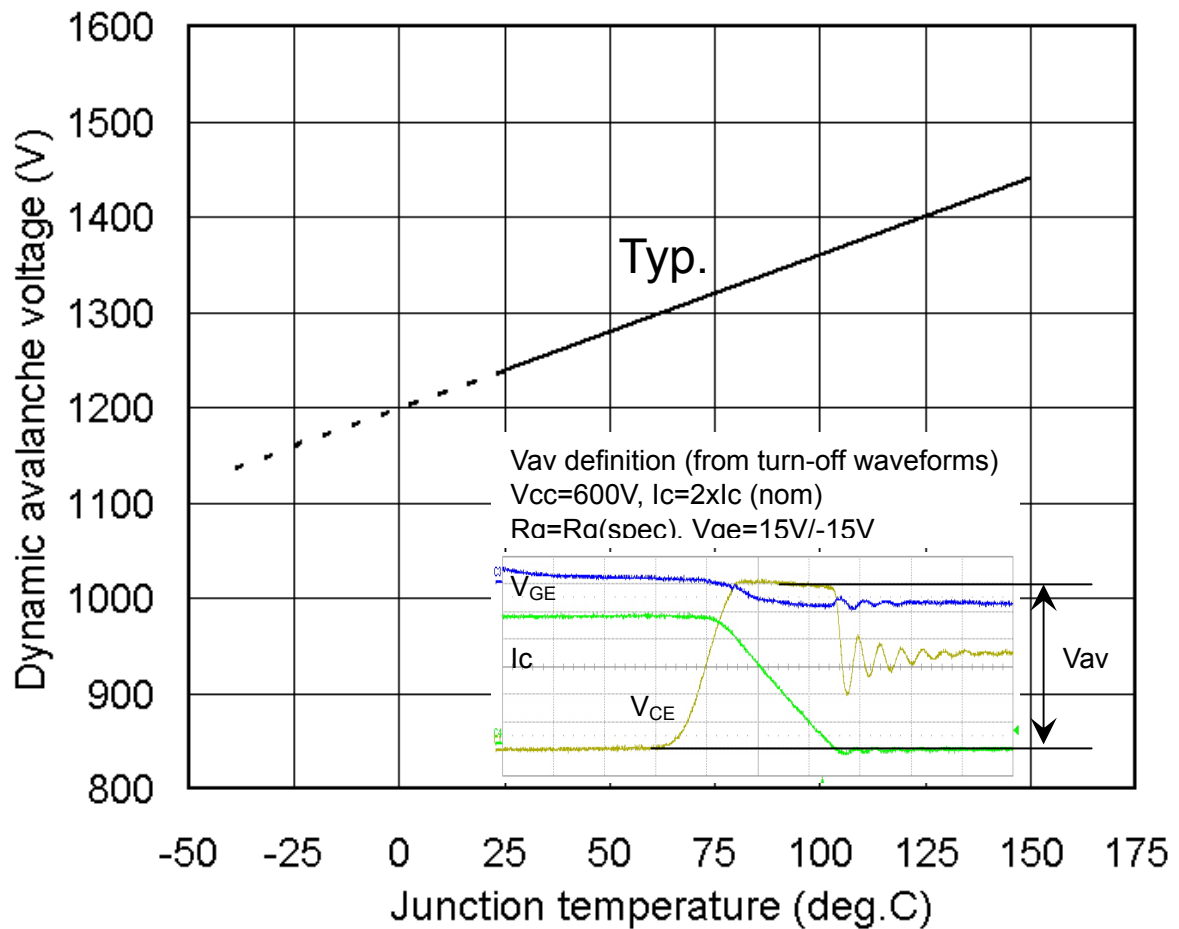


Fig. Dynamic Avalanche Voltage ( $V_{av}$ ) as function of  $T_j$

Technical data: MT5F24330

# - Fuji IGBT Module V Series 1200V Family -

## Parallel connection of 2in1 package modules

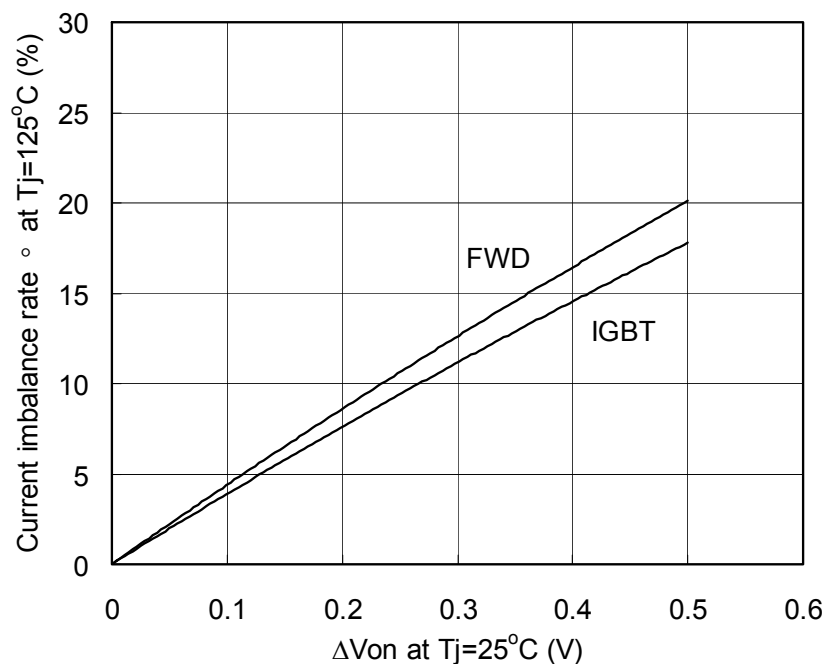
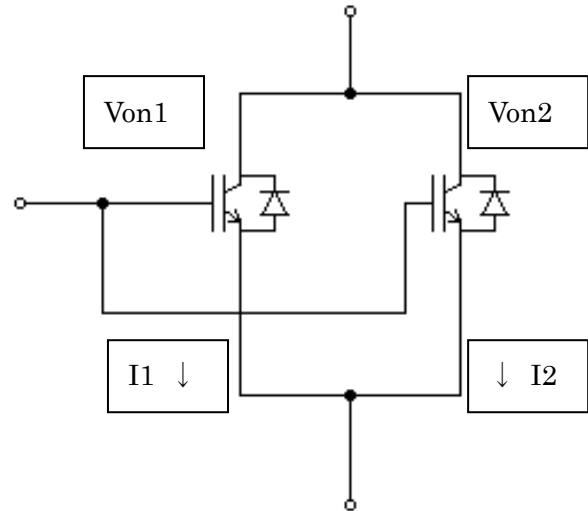
Circuit configuration and formula

$$\Delta V_{on} = |V_{on2} - V_{on1}| \quad (V_{on2} > V_{on1})$$

$$I_{c(ave)} = (I_1 + I_2) / 2$$

Current imbalance is caused by the difference between  $V_{on1}$  and  $V_{on2}$ , and current is divided into  $I_1$  and  $I_2$ . In this case, the current imbalance can be obtained from the following calculating formula.

$$\alpha = \left( \frac{I_1}{I_{C(ave)}} - 1 \right) \times 100 \quad (\%)$$



$\Delta V_{on}$  and current imbalance rate

When  $n$  IGBT modules are connected in parallel, the maximum allowable current  $\Sigma I$  can be expressed in the following formula by using the current imbalance rate  $\alpha$  at two-parallel connection. This maximum allowable current  $\Sigma I$  is used for reference only.

$$\Sigma I = I_{C(max)} \left[ 1 + (n-1) \frac{\left(1 - \frac{\alpha}{100}\right)}{\left(1 + \frac{\alpha}{100}\right)} \right]$$

Technical data: MT5F24335

# - Fuji IGBT Module V Series 1200V Family -

## Short-circuit capacity

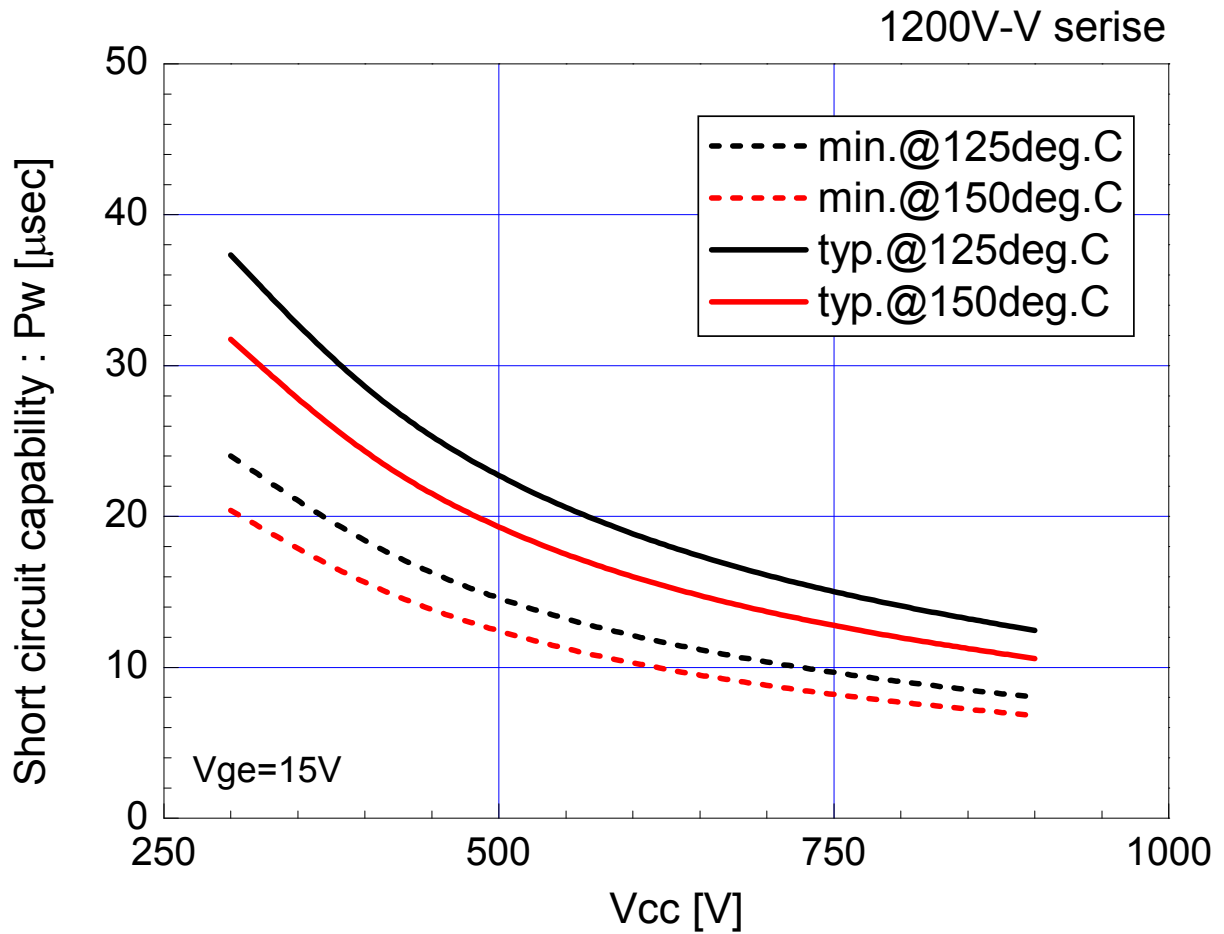


Fig. Relation between applied voltage and short-circuit capacity (1200V Family)

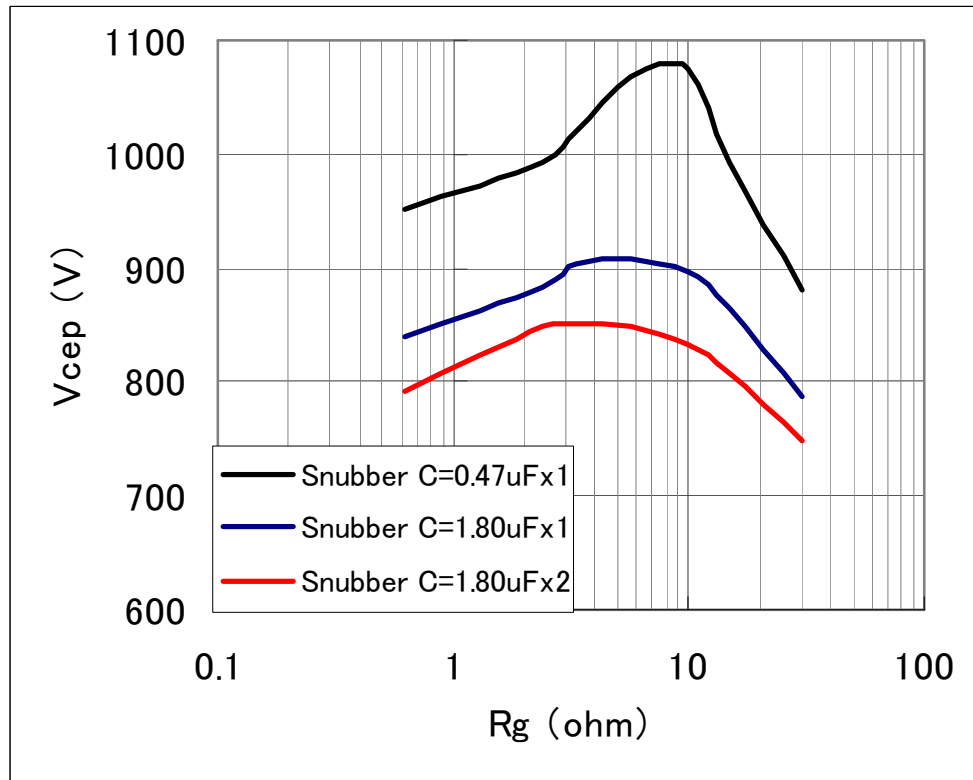
Technical data: MT5F24336

## — Fuji IGBT Module V Series 1200V Family —

### Gate resistance dependence of surge voltage

Type name : 2MBI600VE-120-50

Conditions :  $V_{dc}=600V$ ,  $I_c=600A$ ,  $V_{ge}=\pm 15V$ ,  $T_j=25deg.C$ ,  $R_g=vari.$



Gate Resistance Dependence of Turn-off Surge Voltage

The surge voltage, especially at IGBT turn off, depends on the gate resistance. As shown in the figure above figure shows, the surge voltage is able to control with the gate resistance but the curve shave peaks depending on the junction temperature. The primary reason of such behavior is the interaction of two silicon physics in IGBT chip; 1) the carriers stored in the drift region and 2) Current through MOS channel<sup>1)</sup>.

Reference :

- 1) Y. Onozawa et al., "Investigation of carrier streaming effect for the low spike fast IGBT turn-off", Proc. ISPSD, pp173-176, 2006.

Technical data : MT5F26530

— Fuji IGBT Module V Series 1200V Family —

**Radiation noise comparison by the difference in a gate capacitance connection position**

Type name : 2MBI300VH-120-50

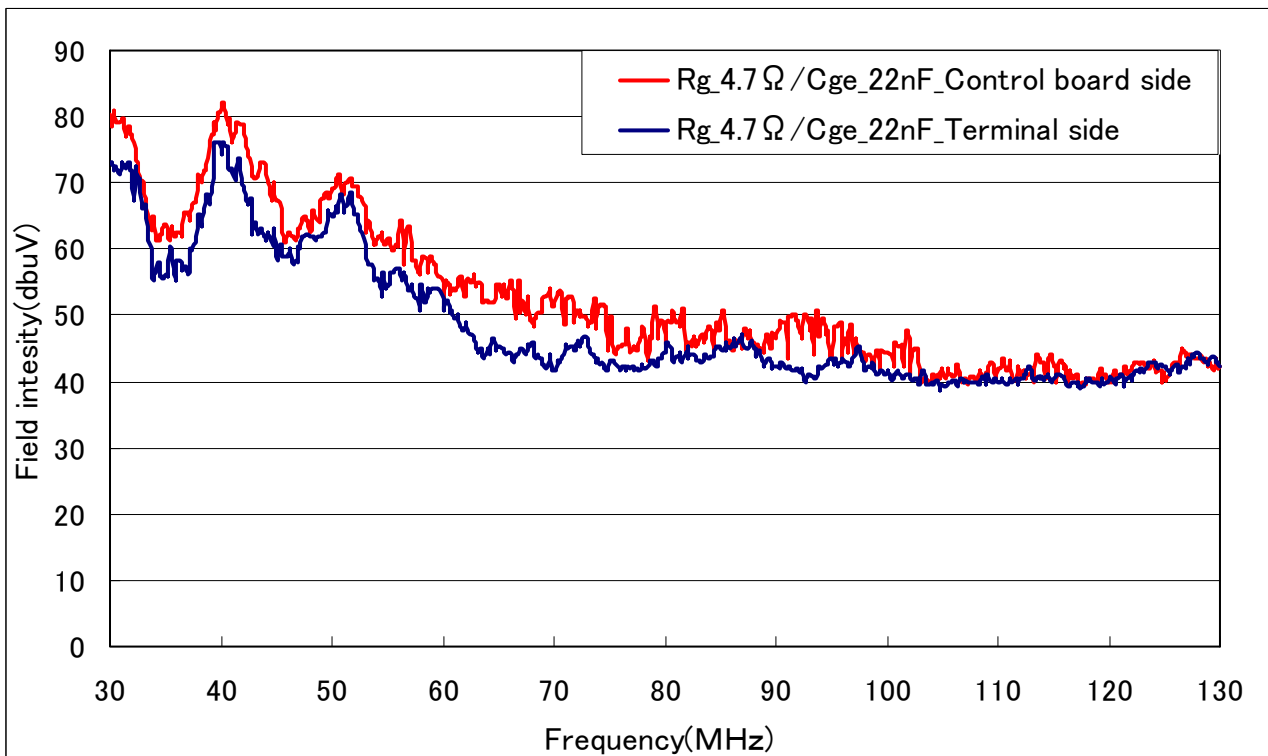
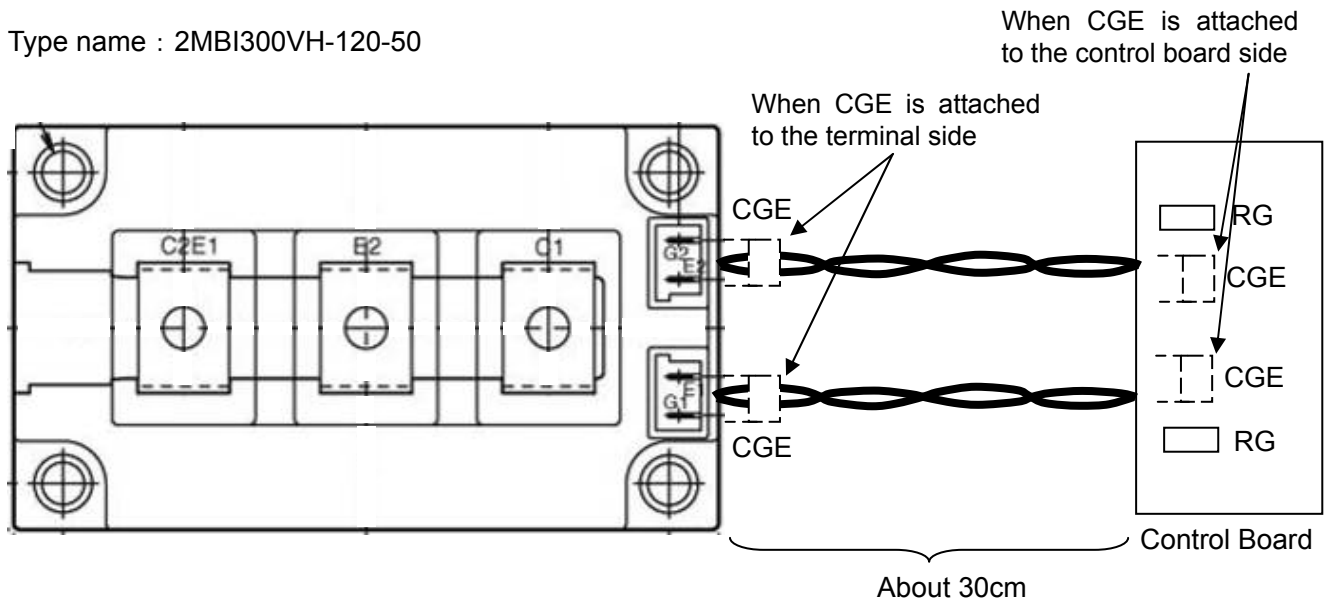


Figure Radiation noise comparison by the difference in a gate capacitance connection position

As shown in the above figure, the higher noise reduction effect is acquired by connecting Cge to the module terminal side.

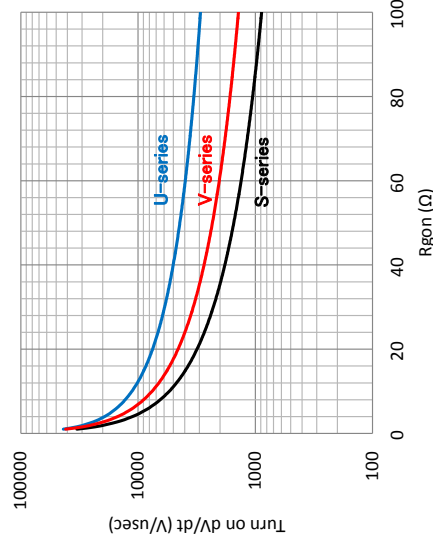
Technical data : MT5F25003

— **Fuji IGBT module S,U,V-series 1200V** —

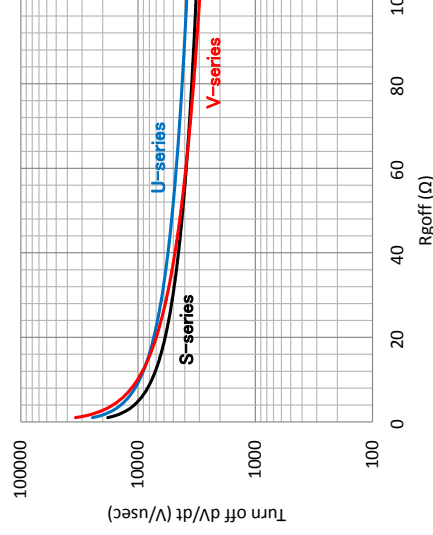
**Rg-dV/dt dependency of S,U,V-series**

Test module : 2MBI75S-120, 2MBI75U4A-120, 2MBI75VA-120-50

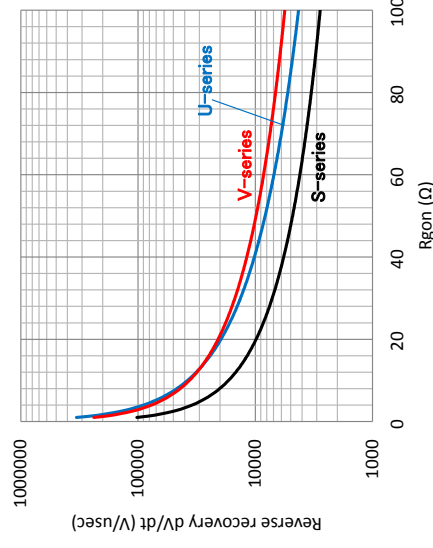
Test condition : V<sub>dc</sub>=600V, I<sub>c</sub>=7.5A (turn on, reverse recovery), 75A (turn off), V<sub>ge</sub>=±1.5V, T<sub>j</sub>=25deg.C, R<sub>g</sub>=vari.



Rgon vs. Turn on dV/dt



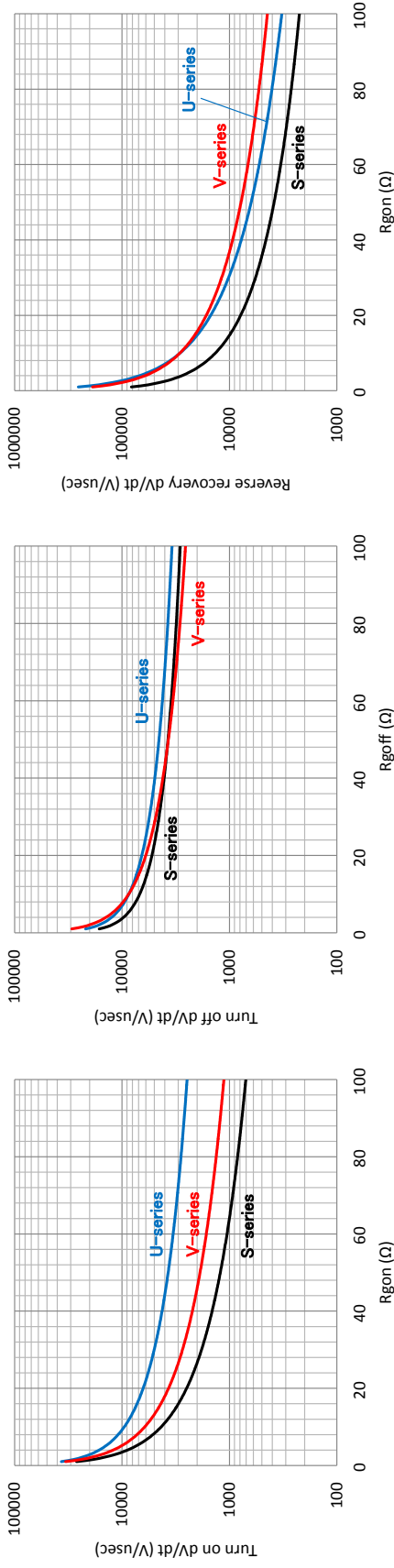
Rgoff vs. Turn off dV/dt



Rgon vs. Reverse recovery dV/dt

Test module : 2MBI100S-120, 2MBI100SC-120, 2MBI100U4A-120-50, 2MBI100VA-120-50

Test condition :  $V_{dc}=600V$ ,  $I_c=10A$ (turn on, reverse recovery),  $100A$ (turn off),  $V_{ge}=\pm 15V$ ,  $T_j=25deg.C$ ,  $R_g=vari.$



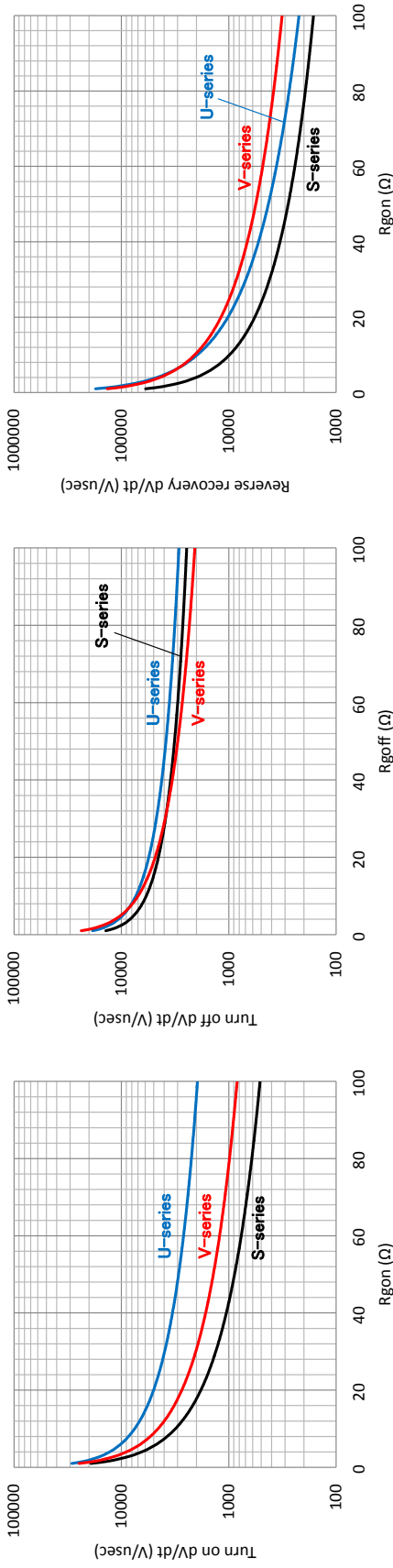
Rgon vs. Turn on dV/dt

Rgoff vs. Turn off dV/dt

Rgon vs. Reverse recovery dV/dt

Test module : 2MBI150S-120, 2MBI150SC-120, 2MBI150U4A-120-50, 2MBI150VA-120-50, 2MBI150VB-120-50

Test condition :  $V_{dc}=600V$ ,  $I_c=15A$ (turn on, reverse recovery),  $150A$ (turn off),  $V_{ge}=\pm 15V$ ,  $T_j=25deg.C$ ,  $R_g=vari.$



Rgon vs. Turn on dV/dt

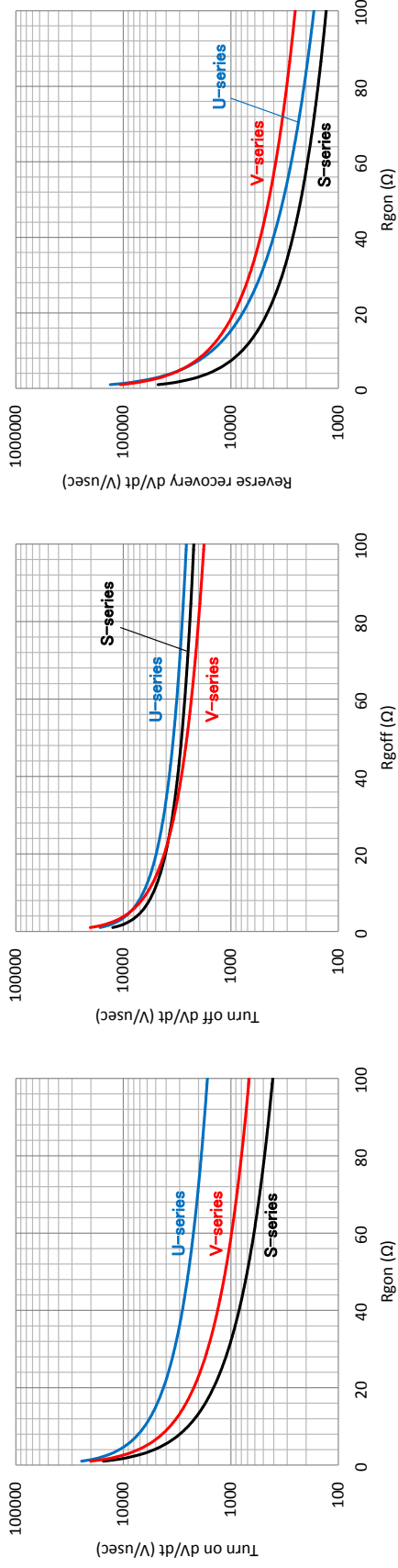
Rgoff vs. Turn off dV/dt

Rgon vs. Reverse recovery dV/dt



Test module : 2MBI200S-120, 2MBI200SB-120, 2MBI200U4B-120-50, 2MBI200U4H-120-50, 2MBI200VB-120-50, 2MBI200VH-120-50

Test condition :  $V_{dc}=600V$ ,  $I_c=20A$ (turn on, reverse recovery), 200A(turn off),  $V_{ge}=\pm 15V$ ,  $T_j=25deg.C$ ,  $R_g=vari.$



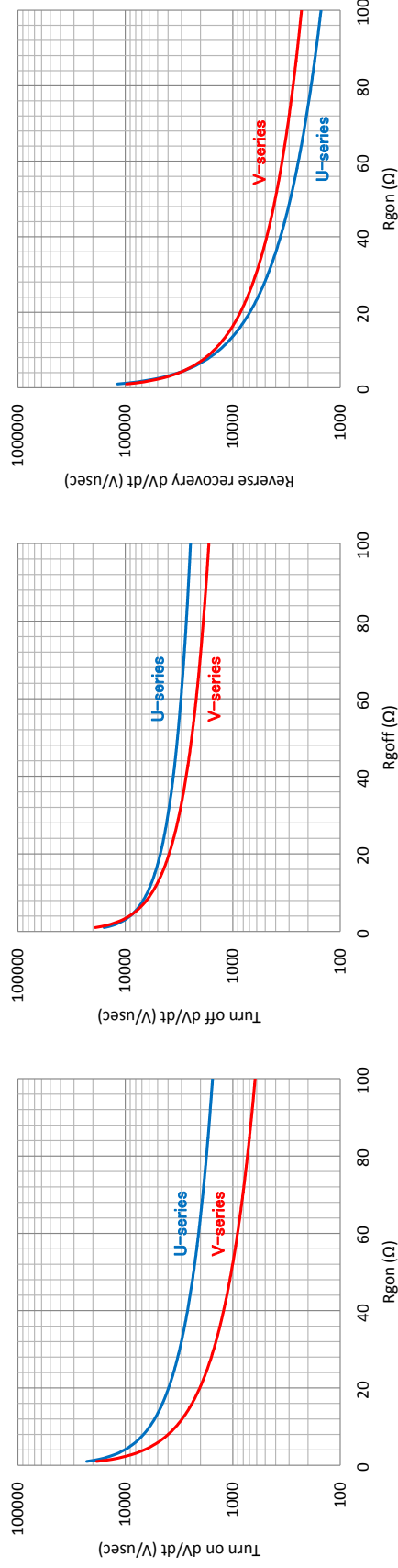
Rgon vs. Turn on dV/dt

Rgoff vs. Turn off dV/dt

Rgon vs. Reverse recovery dV/dt

Test module : 2MBI225U4J-120-50, 2MBI225U4N-120-50, 2MBI225VJ-120-50, 2MBI225VN-120-50

Test condition :  $V_{dc}=600V$ ,  $I_c=22.5A$ (turn on, reverse recovery), 225A(turn off),  $V_{ge}=\pm 15V$ ,  $T_j=25deg.C$ ,  $R_g=vari.$



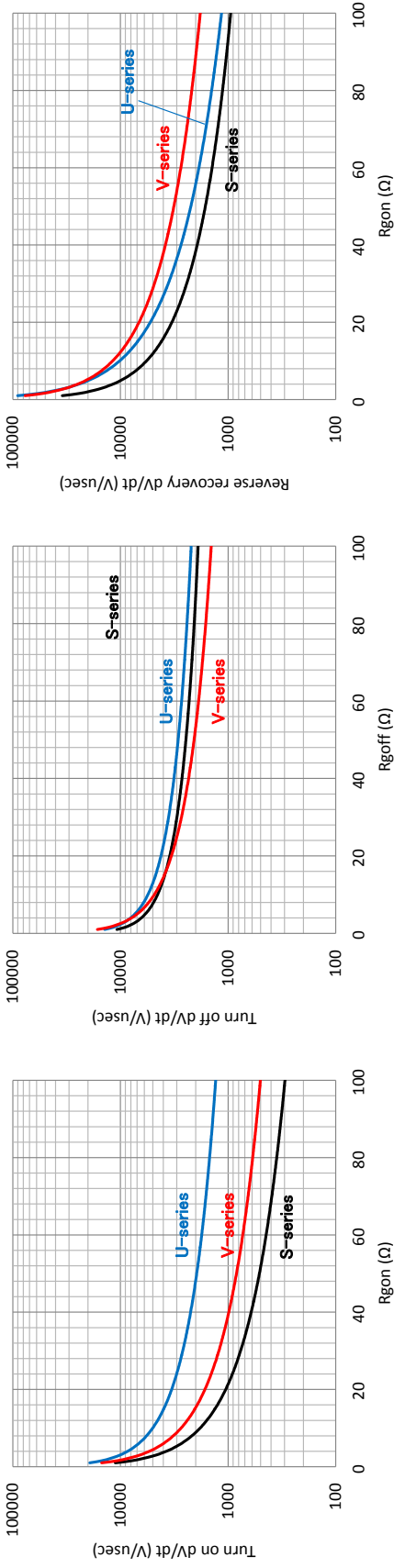
Rgon vs. Turn on dV/dt

Rgoff vs. Turn off dV/dt

Rgon vs. Reverse recovery dV/dt

Test module : 2MBI300S-120, 2MBI300U4D-120-50, 2MBI300U4E-120, 2MBI300U4H-120-50, 2MBI300U4J-120-50, 2MBI300U4N-120-50,  
2MBI300VD-120-50, 2MBI300VE-120-50, 2MBI300VH-120-50, 2MBI300VJ-120-50, 2MBI300VN-120-50

Test condition :  $V_{dc}=600V$ ,  $I_c=30A$ (turn on, reverse recovery),  $300A$ (turn off),  $V_{ge}=\pm 15V$ ,  $T_j=25deg.C$ ,  $R_g=vari.$



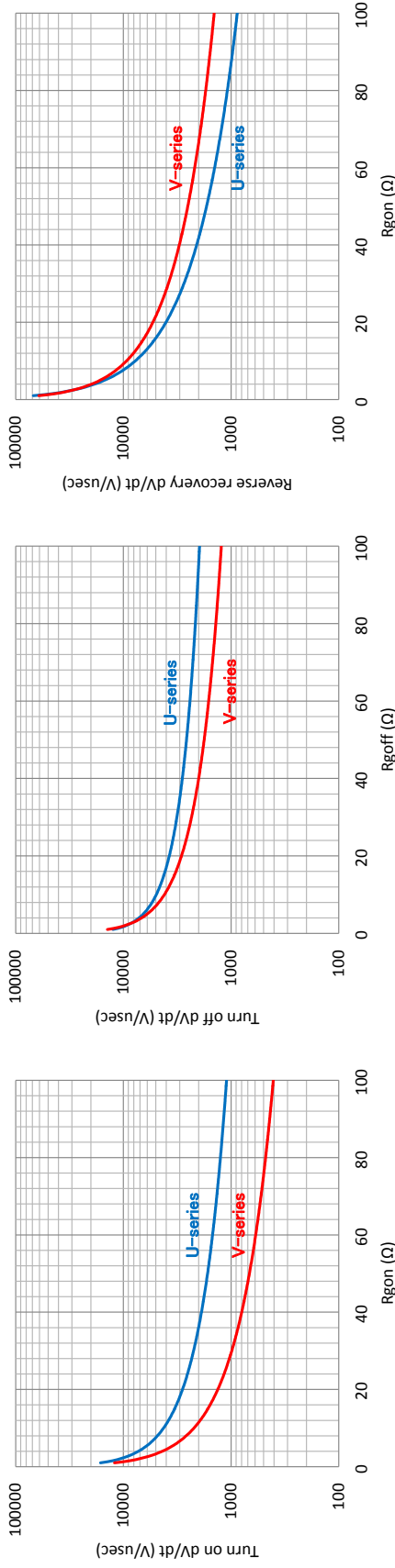
Rgon vs. Turn on dV/dt

Rgoff vs. Turn off dV/dt

Rgon vs. Reverse recovery dV/dt

Test module : 2MBI400U4H-120-50, 2MBI400VD-120-50

Test condition :  $V_{dc}=600V$ ,  $I_c=40A$ (turn on, reverse recovery),  $400A$ (turn off),  $V_{ge}=\pm 15V$ ,  $T_j=25deg.C$ ,  $R_g=vari.$



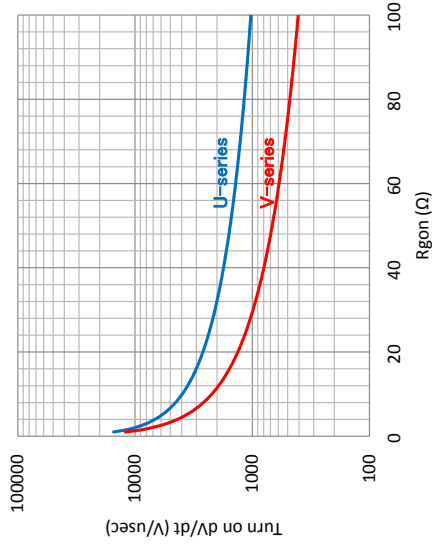
Rgon vs. Turn on dV/dt

Rgoff vs. Turn off dV/dt

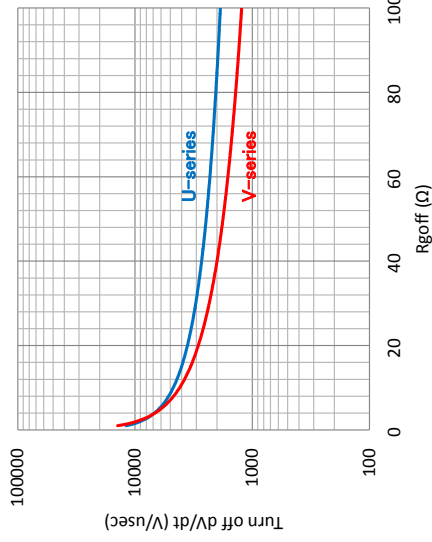
Rgon vs. Reverse recovery dV/dt

Test module : 2MBI450U4E-120, 2MBI450U4J-120-50, 2MBI450U4N-120-50, 2MBI450VE-120-50, 2MBI450VH-120-50, 2MBI450VJ-120-50, 2MBI450VN-120-50

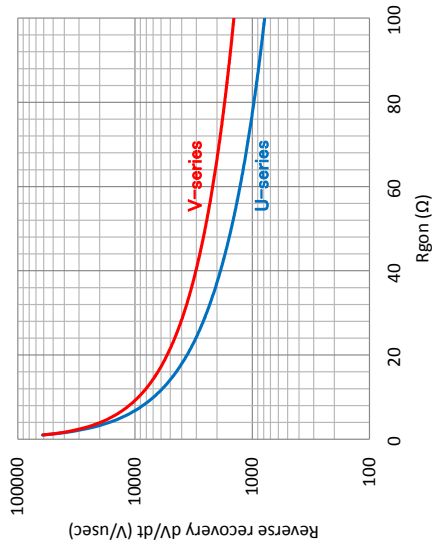
Test condition :  $V_{dc}=600V$ ,  $I_c=45A$ (turn on, reverse recovery),  $450A$ (turn off),  $V_{ge}=\pm 15V$ ,  $T_j=25deg.C$ ,  $R_g=vari.$



Rgon vs. Turn on dV/dt



Rgoff vs. Turn off dV/dt



Rgon vs. Reverse recovery dV/dt

## WARNING

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  - Machine tools
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  - Personal equipment
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  - Traffic-signal control equipment
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