
Fuji IGBT Module V Series 1200V Family

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RBSOA and SCSOA

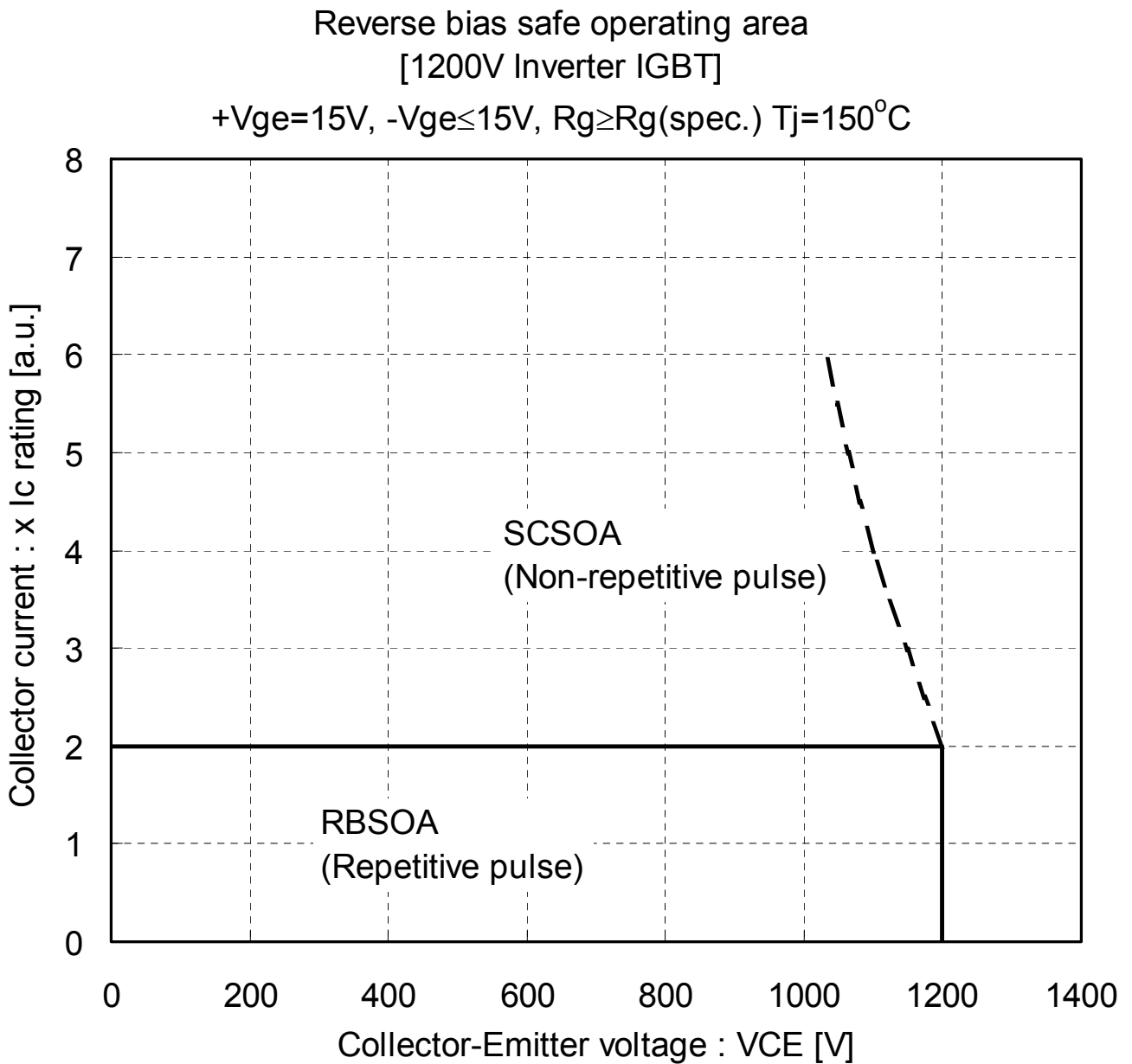


Fig. RBSOA and SCSOA

Technical data: MT5F24325

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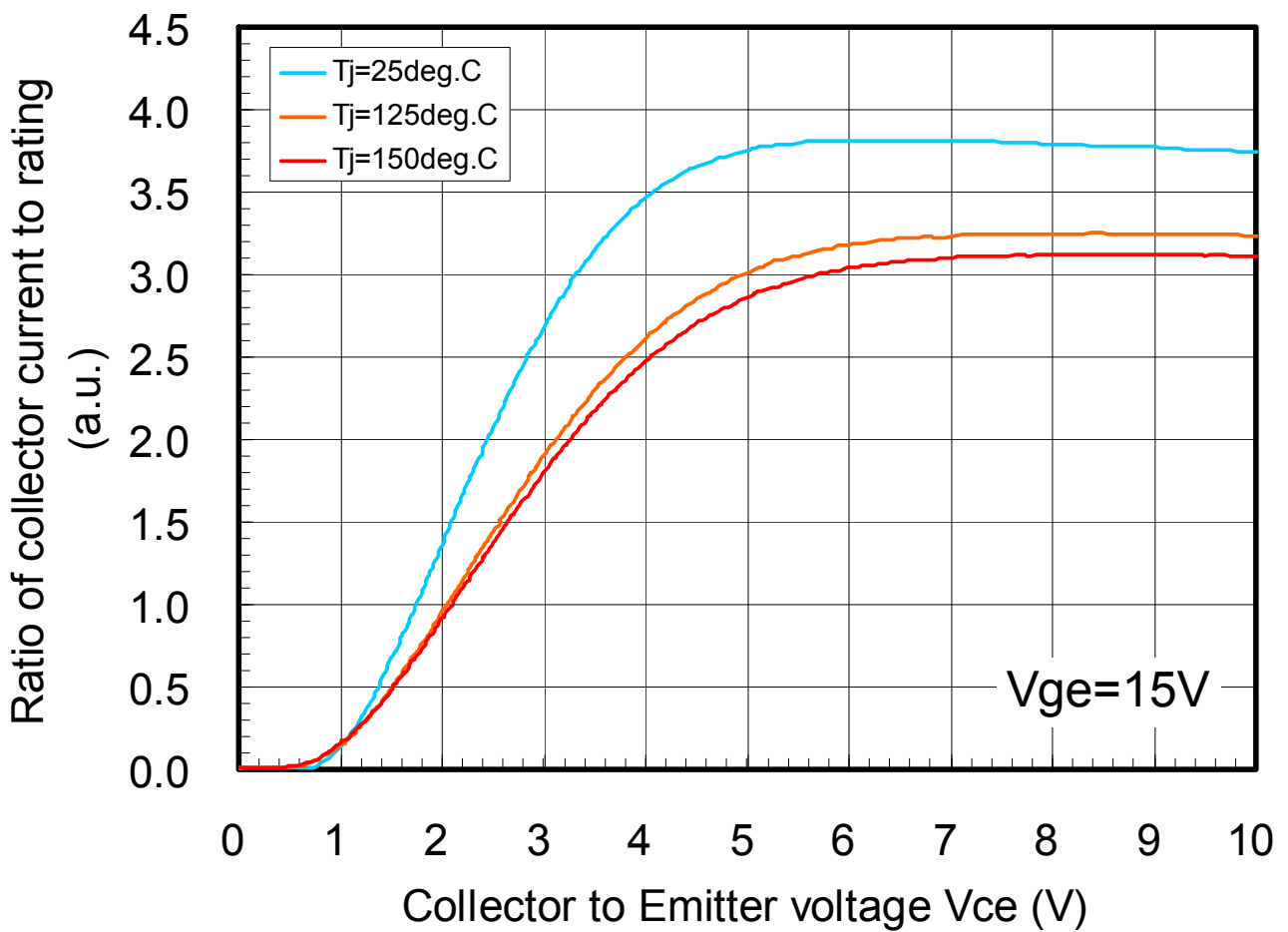
High current output characteristics

V series 1200V product family

Conditions: $T_j = 25^\circ\text{C}$, 125°C and 150°C

$V_{ge} = 15\text{ V}$

Note: This data shows the typical waveforms of chip characteristics. The effect of the internal resistance of the module is not included



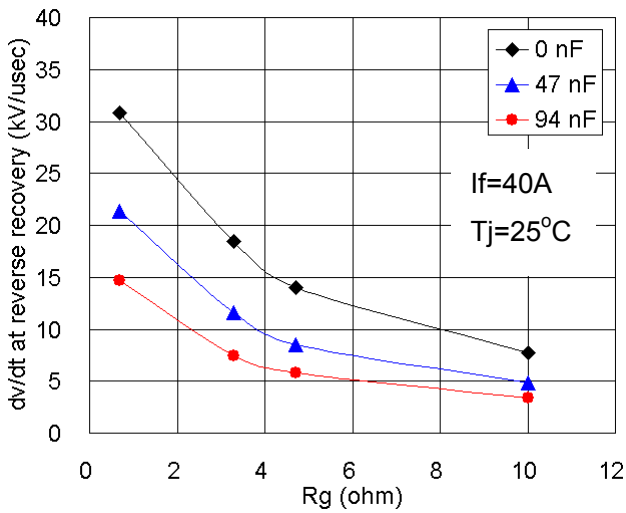
Technical data: MT5F24326

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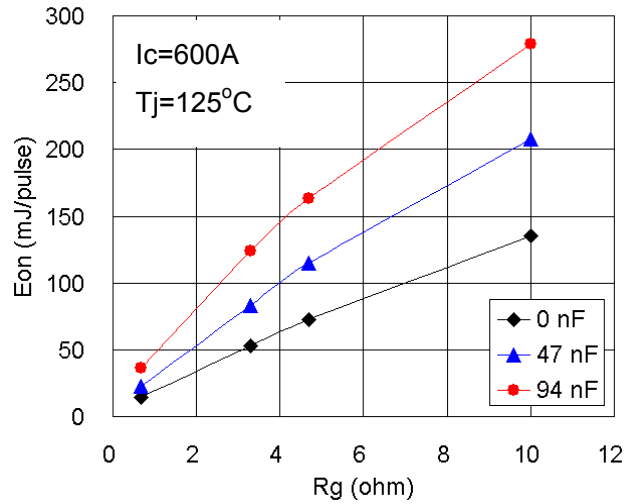
Switching energy and Reverse recovery dv/dt with combination of R_g and C_{ge}

Type name: 2MBI600VN-120-50

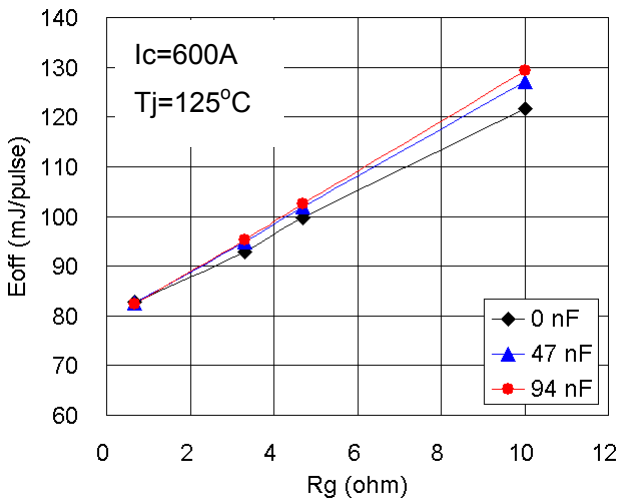
Conditions: $V_{dc}=600V$, I_c , $I_f=40A$ and/or $600A$, $V_{ge}=+/-15V$, $C_{ge}=0, 47, 94nF$,
 $T_j=25^\circ C$ or $125^\circ C$



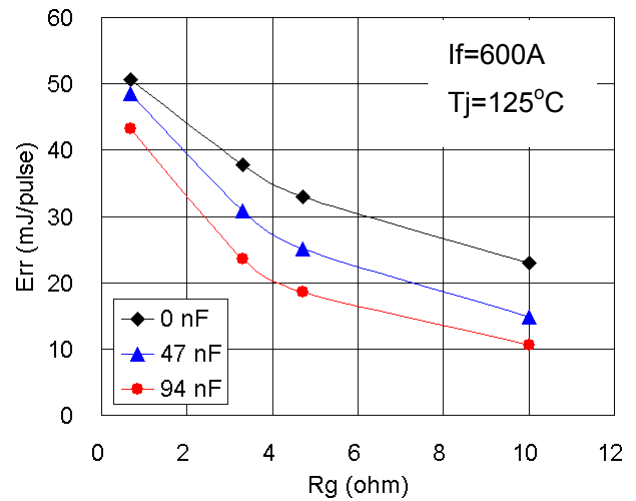
(a) R_g dependence of reverse recovery dv/dt



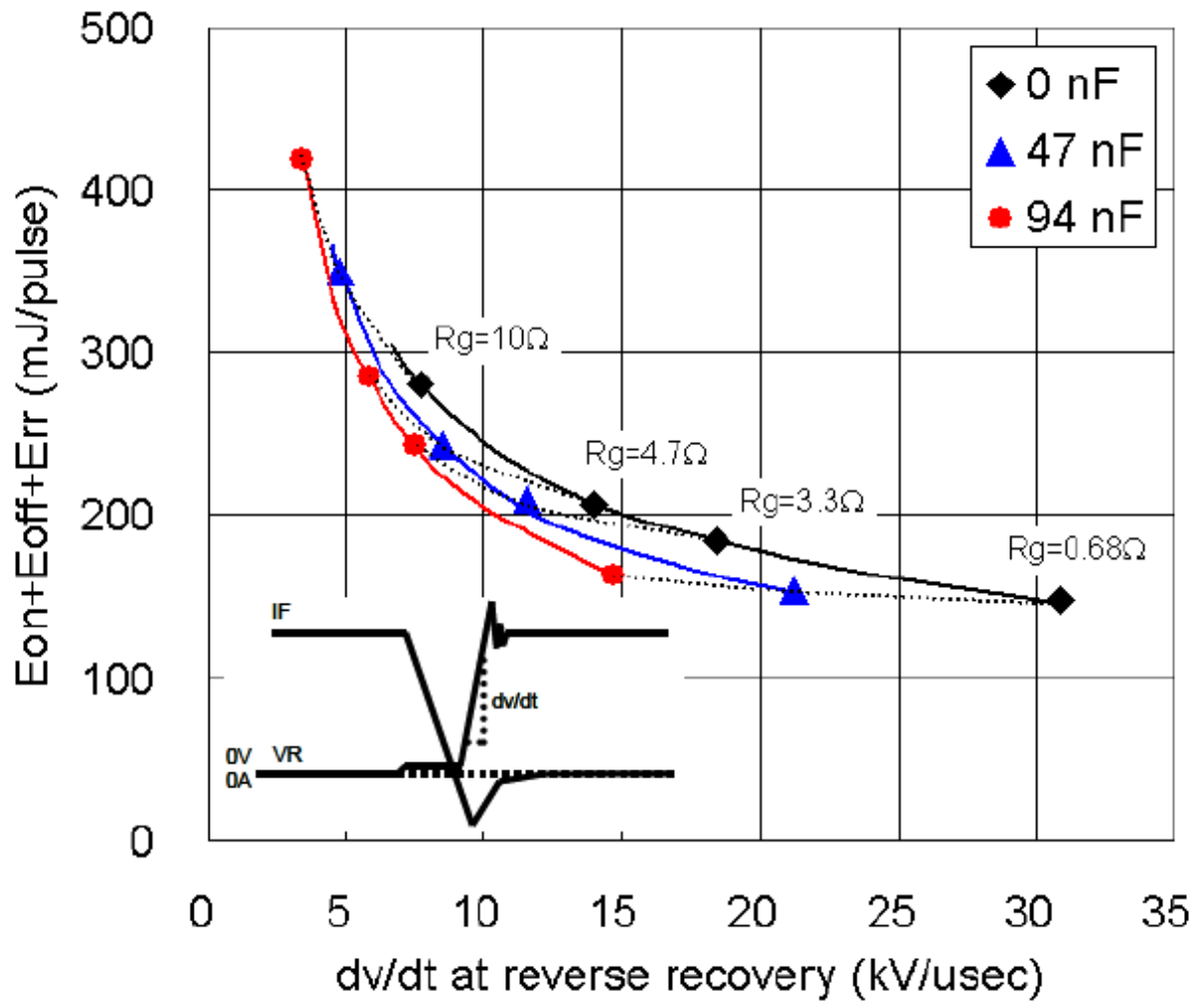
(b) R_g dependence of turn-on loss



(c) R_g dependence of turn-off loss



(d) R_g dependence of reverse recovery loss



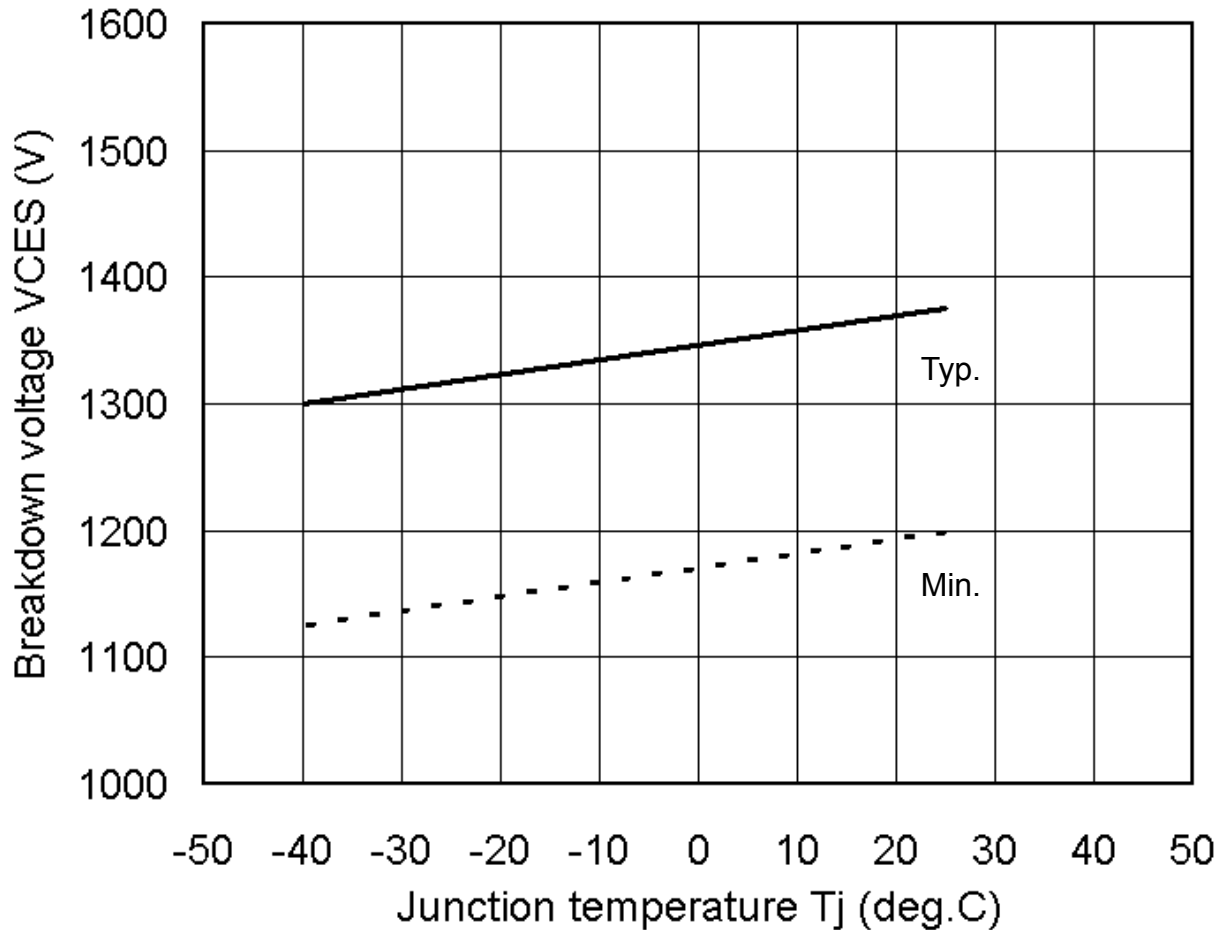
Cge and Rg Dependence for Sum of Switching Loss and Reverse Recovery dv/dt

Additional external capacitance between IGBT gate and emitter terminals has an effect of improving the trade off between reverse recovery dv/dt and total switching energy as shown in above chart. However, simply add C_{ge} slows down the IGBT significantly and it results penalty of increasing the switching loss. Therefore, the combination of extra- C_{ge} and reduction of the gate resistance (R_g) is recommended to achieve the highest performance of lower dv/dt as well as keep switching energy low. Typical C_{ge} and R_g values for initial guess are : 2x of C_{ies} in our datasheet and 1/2 R_g of your original design, however, experimental confirmation in practical application is recommended,

Technical data: MT5F21212

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Junction breakdown voltage V_{CES} and junction temperature T_j



Junction Temperature Dependence of Junction Breakdown Voltage

In General, the breakdown voltage of power semiconductor devices have liner function to the junction temperature if "impact ionization" and "Avalanche multiplication" are dominant physics of junction breakdown. At low temperature, the carriers in drift region are relatively easier to have high velocity because of less scattering due to lattice vibration so that the impact ionization ratio increases. Therefore, the breakdown voltage of the power semiconductor device becomes lower at low temperature. The temperature effect shown in the above figure should be taken into account into practical design not to exceed breakdown voltage if the target application have chances of low temperature operation and/or start-up.

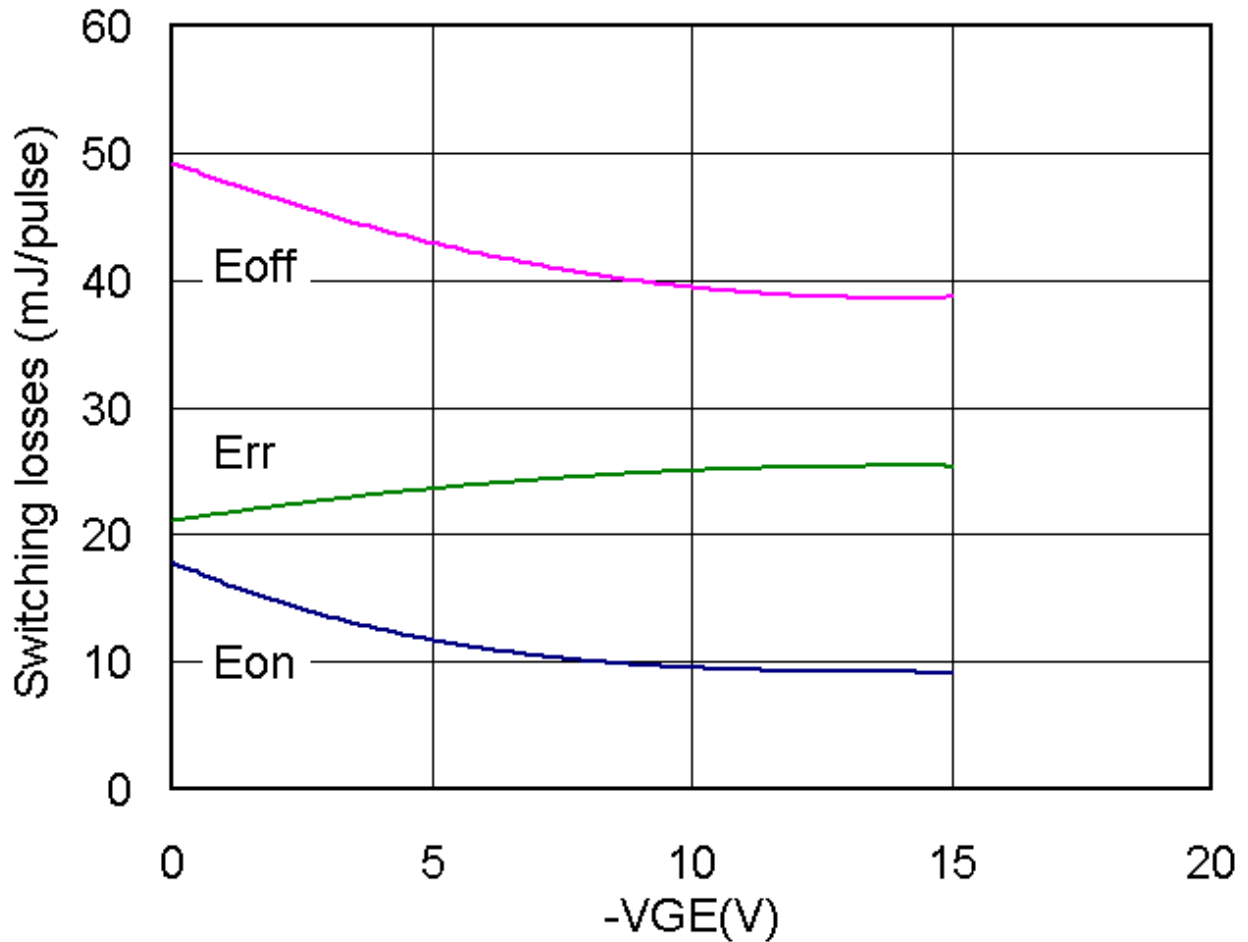
Technical data: MT5F24327

- Fuji IGBT Module V Series 1200V Family -

-Vge and switching loss characteristics

Type name: 2MBI300VN-120-50

Conditions: Vdc=600V, Ic=300A, Vge=+15V, Rg=0.92Ω



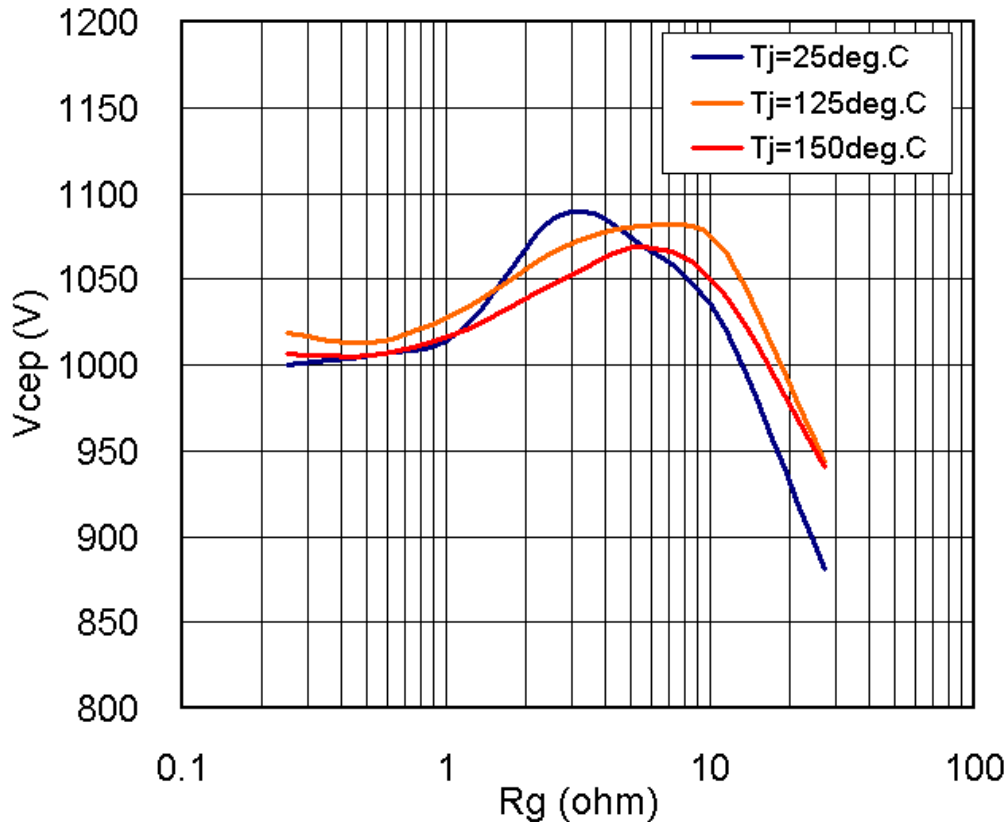
Technical data: MT5F21212

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Gate resistance dependence of surge voltage

Type name: 2MBI450VN-120-50

Conditions: $V_{dc}=600V$, $I_c=450A$, $V_{ge}=\pm 15V$, $L_s=70nH$,



Gate Resistance Dependence of Turn-off Surge Voltage

The surge voltage, especially at IGBT turn off, depends on the gate resistance. As shown in the figure above, the surge voltage can be controlled with the gate resistance, but the curves have peaks depending on the junction temperature. Although detailed reasons for this relation are not described here, the background of such behaviors has already been analyzed and published. The primary reason for such behavior is the interaction of two silicon physics in IGBT chip; 1) the carriers stored in the drift region and 2) Current through MOS channel¹⁾.

This chart also indicates that increasing the gate resistance is not only the method to solve the turn-off spike voltage issue. The decrease of the gate resistance may also have an effect.

Reference :

- 1) Y. Onozawa et al., "Investigation of carrier streaming effect for the low spike fast IGBT turn-off", Proc. ISPSD, pp173-176, 2006.

Technical data: MT5F24328

- Fuji IGBT Module V Series 1200V Family -

- $-di_c/dt$ at turn-off and T_j characteristics

- 2MBI600VN-120-50

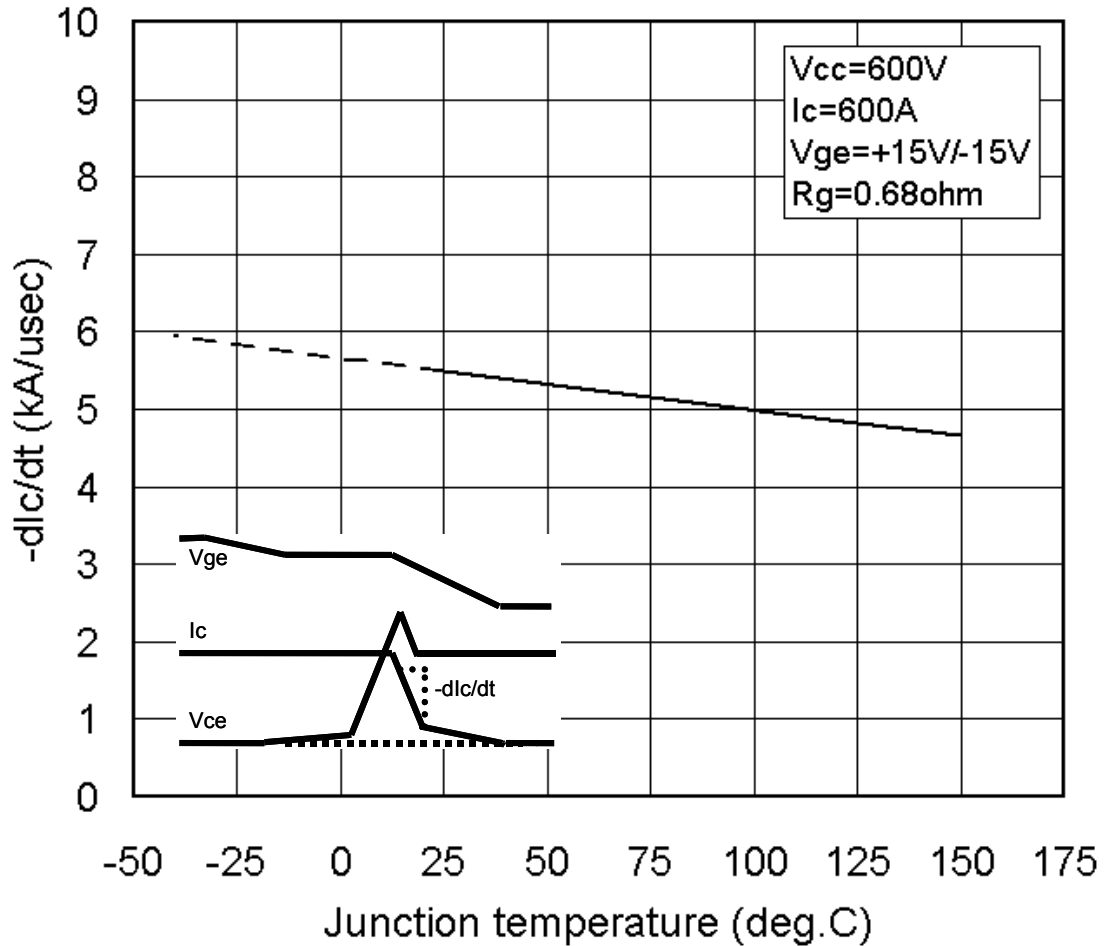


Fig. $-di_c/dt$ at Turn-Off and T_j Characteristics

Technical data: MT5F24329

- Fuji IGBT Module V Series 1200V Family -

Dynamic avalanche voltage V_{av} and T_j characteristics

Type name: 2MBI600VN-120-50

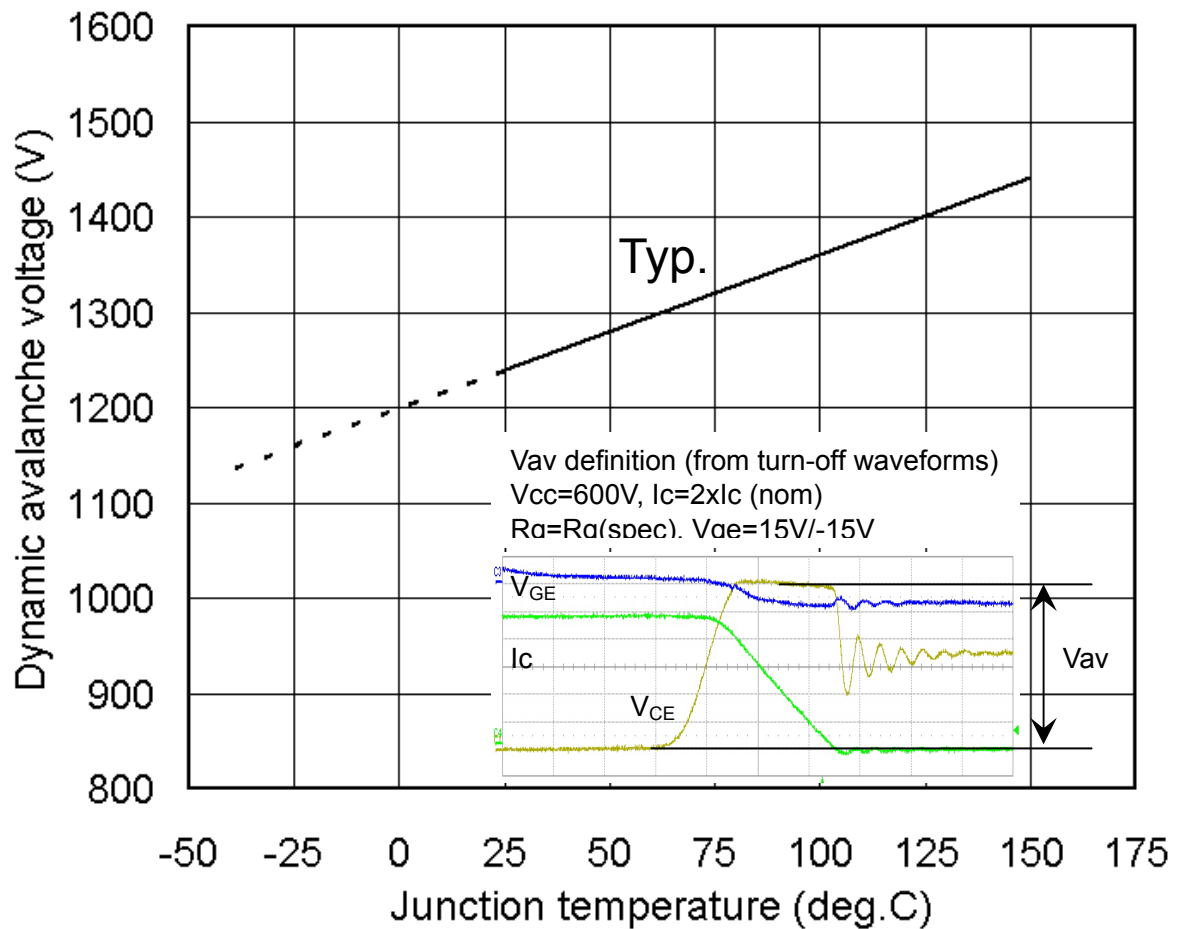


Fig. Dynamic Avalanche Voltage (V_{av}) as function of T_j

Technical data: MT5F24330

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Parallel connection of 2in1 package modules

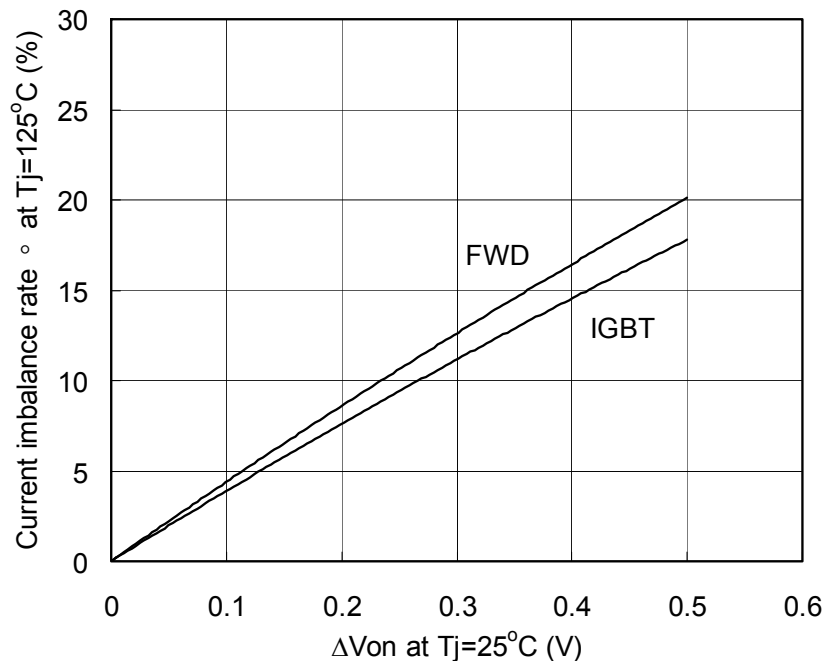
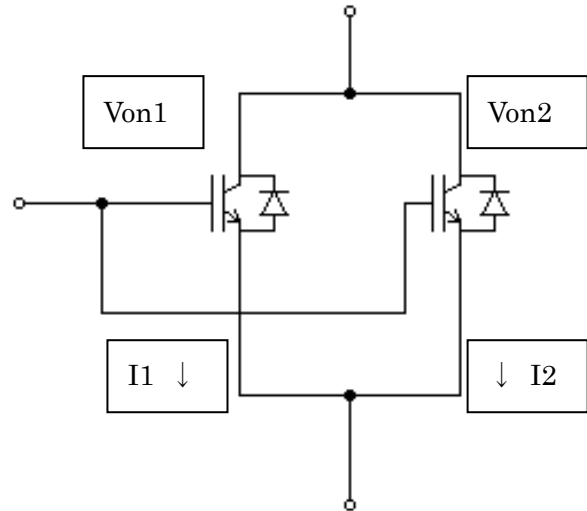
Circuit configuration and formula

$$\Delta V_{on} = |V_{on2} - V_{on1}| \quad (V_{on2} > V_{on1})$$

$$I_{c(ave)} = (I_1 + I_2) / 2$$

Current imbalance is caused by the difference between V_{on1} and V_{on2} , and current is divided into I_1 and I_2 . In this case, the current imbalance can be obtained from the following calculating formula.

$$\alpha = \left(\frac{I_1}{I_{C(ave)}} - 1 \right) \times 100 \quad (\%)$$



Δ Von and current imbalance rate

When n IGBT modules are connected in parallel, the maximum allowable current ΣI can be expressed in the following formula by using the current imbalance rate α at two-parallel connection. This maximum allowable current ΣI is used for reference only.

$$\Sigma I = I_{C(max)} \left[1 + (n-1) \frac{\left(1 - \frac{\alpha}{100} \right)}{\left(1 + \frac{\alpha}{100} \right)} \right]$$

Technical data: MT5F24335

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Short-circuit capacity

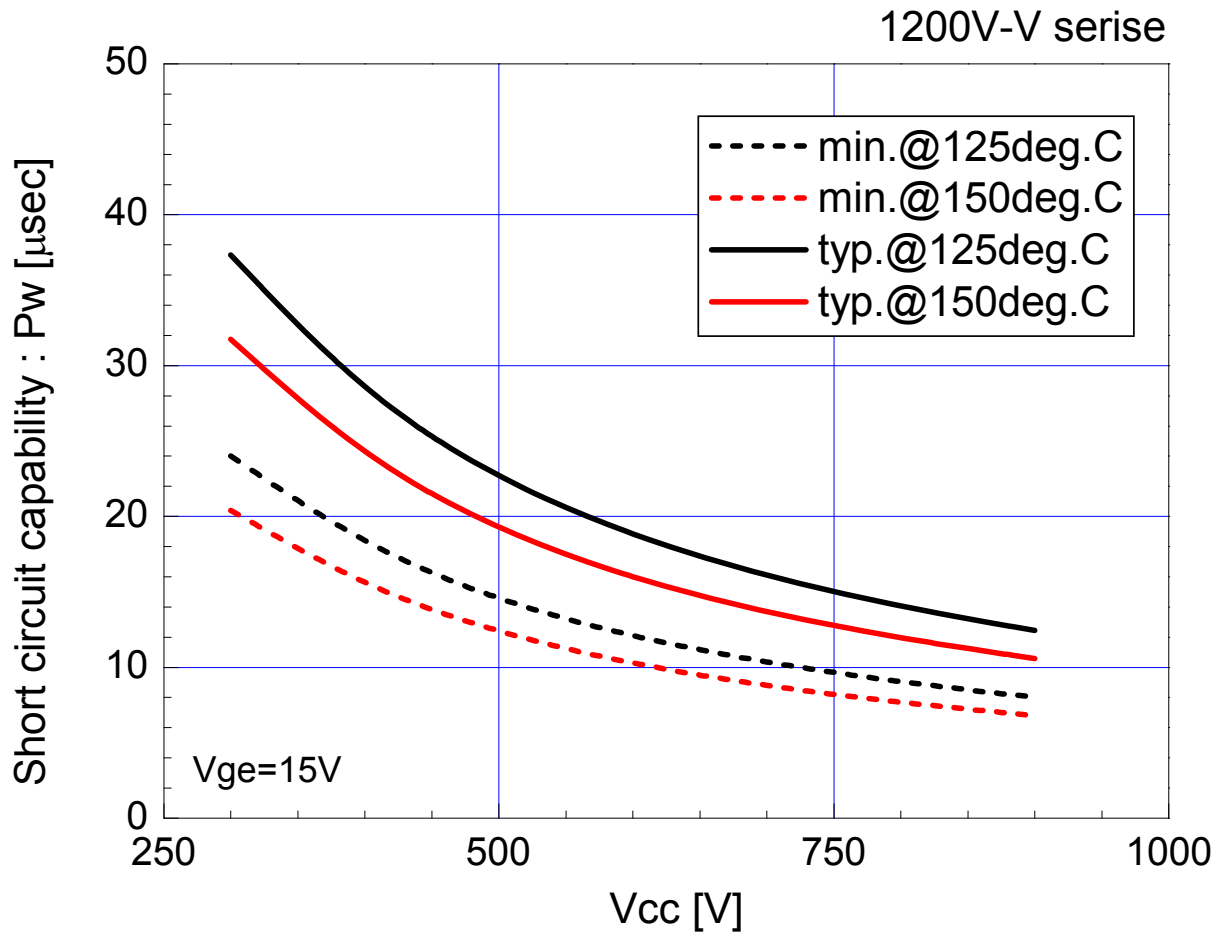


Fig. Relation between applied voltage and short-circuit capacity (1200V Family)

Technical data: MT5F24336

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